

**This Page is Inserted by IFW Indexing and Scanning  
Operations and is not part of the Official Record**

**BEST AVAILABLE IMAGES**

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

- ☐ **BLACK BORDERS**
- ☐ **IMAGE CUT OFF AT TOP, BOTTOM OR SIDES**
- ☐ **FADED TEXT OR DRAWING**
- ☐ **BLURRED OR ILLEGIBLE TEXT OR DRAWING**
- ☐ **SKEWED/SLANTED IMAGES**
- ☐ **COLOR OR BLACK AND WHITE PHOTOGRAPHS**
- ☐ **GRAY SCALE DOCUMENTS**
- ☐ **LINES OR MARKS ON ORIGINAL DOCUMENT**
- ☐ **REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY**
- ☐ **OTHER:** \_\_\_\_\_

**IMAGES ARE BEST AVAILABLE COPY.**

As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.

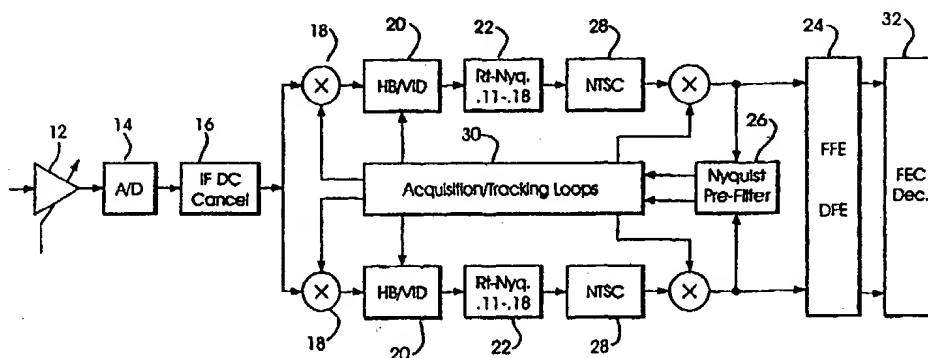
**THIS PAGE BLANK (USPTO)**



## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification <sup>7</sup> : <b>H04L 7/00</b>		<b>A2</b>	(11) International Publication Number: <b>WO 00/27066</b>
			(43) International Publication Date: 11 May 2000 (11.05.00)
(21) International Application Number: PCT/US99/26084		(81) Designated States: AE, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CR, CU, CZ, DE, DK, DM, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, TZ, UA, UG, US, UZ, VN, YU, ZA, ZW, ARIPO patent (GH, GM, KE, LS, MW, SD, SL, SZ, TZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).	
(22) International Filing Date: 3 November 1999 (03.11.99)			
(30) Priority Data: 60/106,921 3 November 1998 (03.11.98) US 60/106,922 3 November 1998 (03.11.98) US 60/106,923 3 November 1998 (03.11.98) US 60/106,938 3 November 1998 (03.11.98) US 60/107,037 3 November 1998 (03.11.98) US 60/107,103 4 November 1998 (04.11.98) US			
(71) Applicant (for all designated States except US): BROADCOM CORPORATION [US/US]; 16215 Alton Parkway, Irvine, CA 99618 (US).		Published Without international search report and to be republished upon receipt of that report.	
(72) Inventors; and (75) Inventors/Applicants (for US only): JAFFE, Steven, T. [US/US]; 21 Sunlight, Irvine, CA 92612 (US). LIU, Tian-Min [CN/US]; 12 Pacific Crest, Laguna Niguel, CA 92677 (US). TAN, Loke, Kun [MY/MY]; 24412 Rue de Monet, Laguna Niguel, CA 92677 (US).			
(74) Agent: ELDREDGE, John, W.; Christie, Parker & Hale, LLP, P.O. Box 7068, Pasadena, CA 91109-7068 (US).			

(54) Title: DUAL MODE QAM/VSB RECEIVER



## (57) Abstract

A television receiver system capable of receiving and demodulating television signal information content that has been modulated and transmitted in accordance with a variety of modulation formats is disclosed. In particular, the system is able to accommodate receipt and demodulation of at least 8 and 16-VSB modulated signals in order to support US HDTV applications, as well as 64 and 256-QAM modulated signals, for European and potential US CATV implementations. The system includes carrier and timing recovery loops adapted to operate on an enhanced pilot signal as well as decision directed carrier phase recovery loops. Phase detectors operate on I and Q rail signals, or generate a Q rail from a Hilbert transform of the I rail. Decision directed loops incorporate a trellis decoder in order to operate on sequence estimated decisions for improved reliability in poor SNR environments.

**FOR THE PURPOSES OF INFORMATION ONLY**

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Armenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav Republic of Macedonia	TM	Turkmenistan
BF	Burkina Faso	GR	Greece	ML	Mali	TR	Turkey
BG	Bulgaria	HU	Hungary	MN	Mongolia	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MR	Mauritania	UA	Ukraine
BR	Brazil	IL	Israel	MW	Malawi	UG	Uganda
BY	Belarus	IS	Iceland	MX	Mexico	US	United States of America
CA	Canada	IT	Italy	NE	Niger	UZ	Uzbekistan
CF	Central African Republic	JP	Japan	NL	Netherlands	VN	Viet Nam
CG	Congo	KE	Kenya	NO	Norway	YU	Yugoslavia
CH	Switzerland	KG	Kyrgyzstan	NZ	New Zealand	ZW	Zimbabwe
CI	Côte d'Ivoire	KP	Democratic People's Republic of Korea	PL	Poland		
CM	Cameroon	KR	Republic of Korea	PT	Portugal		
CN	China	KZ	Kazakstan	RO	Romania		
CU	Cuba	LC	Saint Lucia	RU	Russian Federation		
CZ	Czech Republic	LI	Liechtenstein	SD	Sudan		
DE	Germany	LK	Sri Lanka	SE	Sweden		
DK	Denmark	LR	Liberia	SG	Singapore		
EE	Estonia						

1

## DUAL MODE QAM/VSB RECEIVER

## PRIORITY CLAIM

5

The present application claims the benefit of the priority date of U.S. Provisional Applications Serial Nos. 60/106,921, filed November 3, 1998, 60/106,922, filed November 3, 1998, 60/106,923, filed November 3, 1998, 60/106,938, filed November 3, 1998, 60/107,103, filed November 4, 1998 and 60/107,037, filed November 3, 1998, the entire disclosures of which are expressly incorporated herein by reference.

10

## FIELD OF THE INVENTION

The present invention relates to systems for, and methods of, recovering digitally modulated television signals and, more particularly, to a dual mode QAM/VSB receiver system for recovering quadrature amplitude modulated or vestigial sideband modulated signals.

15

## BACKGROUND OF THE INVENTION

Modern digital telecommunication systems are operating at ever-increasing data rates to accommodate society's growing demands for information exchange. However, increasing the data rates, while at the same time accommodating the fixed bandwidths allocated by the Federal Communications Commission (FCC), requires increasingly sophisticated signal processing techniques. Since low cost, small size and low power consumption are portent in the hardware implementations of such communication systems, custom integrated circuit solutions are important to achieving these goals.

20

Next generation digital television systems, such as cable transported television (CATV) and high-definition television (HDTV) rely on telecommunication transceivers to deliver data at rates in excess of 30 megabits per second (30 Mb/s). The ATSC A/53 Digital Television Standard, was developed by the "Digital HDTV Alliance" of U.S. television vendors, and has been accepted as the standard for terrestrial transmission of SDTV and HDTV signals in the United States. The ATSC A/53 standard is based on an 8-level vestigial sideband (8-VSB) modulation format with a nominal payload data rate of 19.4 Mbps in a 6 MHz channel. A high data rate mode, for use in a cable television environment, is also specified by the standard. This particular mode, defined in Annex D to the ITU-T J.83 specification, utilizes a 16-VSB modulation format to provide a data rate of 38.8 Mbps in a 6 MHz channel.

30

Transmission modes defined in ITU-T J.83 Annex A/C are used primarily outside the United States for digital cable television transmission. The transmission modes supported by this specification have been adopted in Europe as the Digital Video Broadcast for Cable (DVB-C) standard, and further adopted by the Digital Audio-Video Council (DAVIC) with extensions to support 256-QAM modulation formats.

35

1           Beyond these divergent requirements, the ITU-T J.83 Annex B standards define the dominant methodology for digital television delivery over CATV networks in the United States. It has been adopted as the physical layer standard by various organizations including the SCTE DVS-031, MCNS-DOCSIS and the IEEE 802.14 committee.

5           Given the implementation of multiple modulation techniques in the various adopted standards, there exists a need for a television receiver system capable of receiving and demodulating television signal information content that has been modulated and transmitted in accordance with a variety of modulation formats. In particular, such a system should be able to accommodate receipt and demodulation of at least 8 and 16-VSB modulated signals in order to support US HDTV applications, as well as 64 and 256-QAM modulated signals, for European and potential US CATV implementations.

#### SUMMARY OF THE INVENTION

15           In one aspect, the invention is directed to a digital communication system for receiving signals modulated in accordance with a multiplicity of modulation formats. The system includes a front end, receiving an input spectrum at an intermediate frequency, first and second nested carrier tracking loops and a symbol timing loop, where the tracking and timing loops control reference synthesizer circuits in operative response to a passband signal centered at a frequency characteristic of an inserted pilot signal. The passband signal contemplates a pair of symmetric signals, each of the symmetric signals centered at the characteristic frequency of the pilot signal and where each of the symmetric signals includes an augmented pilot signal.

20           In a further aspect, the invention is directed to a digital communication system for receiving signals modulated in accordance with a multiplicity of modulation formats and includes a front end receiving an input spectrum at an intermediate frequency; first and second nested carrier tracking loops, the first loop acquiring carrier frequency lock in operative response to a pilot frequency component inserted into the received spectrum, the second loop providing a signal adapted to position the spectrum at a predetermined location relative to baseband in operative response to said pilot frequency component; a third tracking loop coupled to define a symbol timing parameter in operative response to said same pilot frequency component; an equivalent filter operating on the received spectrum in order to define a pair of symmetric signals, each of the symmetric signals centered at the characteristic frequency of the pilot frequency component when the received spectrum is at baseband; and a decision directed carrier recovery loop having a phase detector operative with respect to each of the multiplicity of modulation formats.

30           In another aspect, the invention is directed to a digital communication system for receiving signals modulated in accordance with a multiplicity of modulation formats, including a front end receiving an input spectrum at an intermediate frequency; first and second nested carrier tracking loops, the first loop acquiring carrier frequency lock in operative response to a predetermined

1 frequency component inserted into the received spectrum, the second loop providing a signal  
adapted to position the spectrum at a predetermined location relative to baseband in operative  
response to said predetermined frequency component; and a third tracking loop coupled to define  
5 a symbol timing parameter in operative response to the same predetermined frequency  
component.

The system also includes an equivalent filter operating on the received spectrum in order  
to define a pair of symmetric signals, each of the symmetric signals centered at the characteristic  
frequency of the predetermined frequency component when the received spectrum is at baseband;  
a decision directed carrier phase recovery loop having a phase detector operative with respect to  
10 each of the multiplicity of modulation formats; a single bit LMS derotator coupled to adjust phase  
offset of signals directed to an adaptive decision feedback equalizer.

The system also includes an adaptive decision feedback equalizer, including a  
feedforward filter a decision feedback filter and a maximum likelihood sequence estimation  
circuit, coupled to receive input symbol samples from the feedforward filter, the maximum  
15 likelihood sequence estimation circuit integrated into a timing loop so as to provide enhanced  
reliability symbolic decisions to an input of the timing loop.

The system also includes a first derotator, coupled into the signal path in a position after  
the front end, the derotator converting the received spectrum to a position relative to baseband  
signal in response to the first tracking loop; a variable rate interpolator; an NTSC interference  
20 rejection filter; a square root Nyquist filter, coupled into the signal path in a position after the  
NTSC interference rejection filter; and a second derotator coupled into the signal path in a  
position after the square root Nyquist filter, the second derotator adjusting the received spectrum  
to a baseband signal in response to the second tracking loop.

In a further aspect, the invention is directed to an integrated circuit receiver operating on  
25 a constellation of complex symbols, each symbol capable of representation by a digital word  
having a wordlength  $N$  of bits, the receiver includes a feedback filter, constructed to receive an  
input stimulus signal having a wordlength of  $N-1$  bits the feedback filter outputting a signal  
having a wordlength of  $N-1$  bits; a correction filter constructed to provide an output signal having  
a single bit representation; and means for combining the feedback filter output and the correction  
30 filter output to define a signal having a value consistent with an  $N$ -bit representation.

In another aspect of the invention, an integrated circuit receiver operates on a constellation  
of complex symbols, with each symbol represented by a number  $N$  of bits. The receiver includes  
an adaptive decision feedback equalizer, in turn, including a decision feedback filter,  
constructed to receive a symbol decision having a wordlength of  $N-1$  bits, the decision feedback  
35 filter outputting a compensated symbol decision having a wordlength of  $N-1$  bits, an offset  
generation circuit, generating a DC value corresponding to an  $N$ th bit representation, and a  
summing circuit for combining the decision feedback filter output and the DC value generated  
by the offset generation circuit to recover an  $N$  bit symbol.

1 In yet another aspect, the invention relates to an integrated circuit receiver which includes  
at least one timing loop; a decision feedback equalizer, in turn, including a feedforward filter and  
a decision feedback filter; and a maximum likelihood sequence estimation circuit, coupled  
5 to receive input symbol samples from the feedforward filter, the maximum likelihood sequence  
estimation circuit integrated into the timing loop so as to provide enhanced reliability symbolic  
decisions to an input of the timing loop.

In a further aspect, the invention relates to an integrated circuit which includes a decision  
directed symbol error magnitude determination circuit; a symbol rotation direction indication  
circuit; and where the symbol error magnitude circuit is operative in response to a first-phase  
10 portion of a complex signal, and where the symbol rotation direction indication circuit is  
operative in response to a Hilbert transform of the first-phase portion.

In another aspect, the invention relates to an integrated circuit receiver including a decision  
directed carrier phase recovery circuit for complex signals representing symbols characterized  
by in-phase and quadrature-phase portions separated in time by an offset. The carrier phase  
15 recovery circuit includes a sampling circuit configured to sample each of the in-phase and  
quadrature-phase portions of the complex signal at an in-phase sampling time and at a  
quadrature-phase sampling time separated by an offset; a separation circuit, connected to separate  
the sampled, in-phase, signal into an in-phase sample time data stream and an in-phase time  
offset data stream; a decision circuit, connected to receive the in-phase sample time data stream  
20 and generate a tentative symbolic decisions from in-phase sampled data; a summing circuit  
coupled to combine the tentative symbolic decisions with signals from the in-phase sample time  
data stream to generate an in-phase symbolic error term; and a multiplier circuit connected to  
combine the in-phase symbolic error term with a time offset signal representing the quadrature-  
phase portion of the complex signal.

#### 25 BRIEF DESCRIPTION OF THE DRAWINGS

These and other features, aspects and advantages of the present invention will be more  
fully understood when considered with respect to the following detailed description, appended  
claims and accompanying drawings wherein:

30 FIG. 1 is a simplified, semi-schematic block diagram of a dual mode QAM/VSB receiver  
architecture in accordance with the invention;

FIG. 2 is a graphical representation of QAM, VSB and offset-QAM spectra subtended by  
their respective eye diagrams illustrating both the I and Q rails;

35 FIG. 3 illustrates a typical 6 MHz spectra represented as a raised cosine waveform  
illustrating transition regions and the location of a pilot signal;

FIG. 4 is a simplified, semi-schematic block diagram of the architecture of carrier recovery  
and baud loops of a dual mode QAM/VSB receiver in accordance with the invention;



- 1        FIG. 5 is a simplified, semi-schematic block diagram of a square root Nyquist low pass filter in combination with a Nyquist high pass prefilter expressed as an equivalent bandpass filter;
- FIG. 6 is a graphical representation of the affects of the low pass, high pass and equivalent bandpass filters of FIG. 5 on an input spectrum, where the filter's cutoff frequencies have an integer relationship to the sampling frequency;
- 5        FIG. 7 is a simplified, semi-schematic block diagram of a baud loop as might be implemented in a dual mode QAM/VSF receiver architecture in accordance with the invention;
- FIG. 8 is a simplified, semi-schematic block diagram of a phase detector as might be implemented in the baud loop of FIG. 7;
- 10       FIG. 9 is a simplified, semi-schematic block diagram of a dual mode QAM/VSF receiver architecture, including decision directed carrier phase tracking circuitry in accordance with the invention;
- FIG. 10 is a simplified, semi-schematic block diagram of a QAM phase detector suitable for implementation in the dual mode QAM/VSF receiver architecture of FIG. 9;
- 15       FIG. 11 is a simplified, semi-schematic block diagram of a VSB phase detector, where the Hilbert transform of an input signal is provided directly;
- FIG. 12 is a simplified, semi-schematic block diagram of a VSB phase detector where the Hilbert transform of an input signal is provided within the phase detector;
- FIG. 13 is a simplified, semi-schematic block diagram of a single bit derotater provided at the equalizer input of the dual mode QAM/VSF system of FIG. 9;
- 20       FIG. 14 is a simplified, semi-schematic block diagram of a decision feedback equalizer;
- FIG. 15 is a simplified block diagram of an exemplary 8-tap decision feedback filter;
- FIG. 16 is a simplified semi-schematic block diagram of a complex decision feedback or complex decision feedforward filter;
- 25       FIG. 17 is a graphical representation of a 256 QAM constellation;
- FIG. 18 is a simplified, semi-schematic block diagram of a decision feedback equalizer including computational offset correction circuitry in accordance with the invention configured for QAM modulated signals;
- FIG. 19 is a simplified, semi-schematic block diagram of a decision feedback equalizer including a pilot tone generation circuit;
- 30       FIG. 20 is a simplified, semi-schematic block diagram of a decision feedback equalizer in accordance with the invention including offset correction circuitry for VSB modulated signals;
- FIG. 21 is a simplified, semi-schematic block diagram of a trellis encoder including a symbol mapper suitable for 8 VSB transmission;
- 35       FIG. 22 is a simplified, semi-schematic block diagram of a decision feedback equalizer circuit, including carrier and timing loops and a symbol-by-symbol slicer;

1           FIG. 23 is a simplified, semi-schematic block diagram of a decision feedback equalizer circuit, including carrier and timing loops and a TCM decoder circuit in accordance with the invention;

5           FIG. 24 is a simplified, semi-schematic block diagram of a decision feedback equalizer circuit depicting the construction and arrangement of a TCM decoder circuit in accordance with the invention;

          FIG. 25 is a simplified, semi-schematic block diagram of a 4-state traceback path memory circuit suitable for practice of the present invention.

## 10   DETAILED DESCRIPTION OF THE INVENTION

          The present invention is directed to digital data communication systems and methods for operating such systems in order to synchronize a receiver's timebase to a remote transmitter's. Carrier frequency and symbol timing information is recovered from a pilot (unsuppressed carrier) signal that is inserted into a VSB spectrum, in contrast to conventional timing recovery systems, which recover timing information from the segment sync signal that is provided at the end of every line of 828 symbols, and is specifically designed to facilitate timing recovery.

15           In a first aspect of the invention, a digital communication system includes an analog front end which receives an input spectrum in an intermediate frequency. The input spectrum includes an inserted pilot signal, representing a pre-determined frequency component. First and second nested tracking loops are provided, with the first loop acquiring carrier frequency lock in operative response to the predetermined frequency component. The second loop provides a signal adapted to position the input spectrum at a predetermined location relative to baseband in operative response to the predetermined frequency component. A third tracking loop is coupled so as to define a symbol timing parameter in operative response to the same predetermined frequency component. The digital communication system includes an equivalent filter which operates on the received spectrum in order to define a pair of symmetric signals, each of the symmetric signals centered at the characteristic frequency of the predetermined frequency component when the received spectrum is at baseband.

20           In an additional aspect of the invention, the equivalent filter is constructed of a first, high pass filter, having a lower cut-off frequency which is related to the system's sampling frequency. The equivalent filter further includes a second, low pass, filter which has an upper cut-off frequency bearing the same relationship to the sampling frequency as the high pass filter. The first and second filters therefore define an equivalent band pass filter having symmetric passband regions centered about a frequency bearing the same relationship to the sampling frequency. When the received spectrum exhibits a raised cosine response characteristic, the passband regions incorporate the transition regions of the high and low pass filtered spectra.

35           The pilot signals provided at a characteristic predetermined frequency  $f_c$ . In one particular embodiment of the invention, the sampling frequency  $f_s$  is chosen such that the pilot frequency

1 is equal to  $f_s/4$ . The high pass filter accordingly has a lower cut-off of  $f_s/4$  and a passband center  
of about  $f_s/2$ . The low pass filter has an upper cut-off of about  $f_s/4$ , the equivalent filter passband  
is thereby centered at a frequency of  $f_s/4$ . Since one-fourth the sampling frequency, i.e.,  $f_s/4$ , is  
5 designed to be equal to the pilot frequency  $f_c$ , the equivalent filter passband regions are centered  
at  $f_c$  when  $f_c = f_s/4$ .

In a further aspect of the invention, an equivalent filter passband signal is provided to a  
phase/frequency detector which is constructed so as to determine whether the pilot signal is  
centered in the passband region. An oscillator circuit develops a timing reference signal having  
a frequency related to the sampling frequency, the oscillator circuit increasing or decreasing the  
10 timing reference signal frequency in operative response to the position of the pilot signal with  
respect to the passband region center.

A system according to the invention might thus be characterized as including a filter  
circuit for isolating an inserted pilot signal; a detector circuit coupled to receive the isolated pilot  
signal and compare its frequency value to a predetermined frequency; a frequency reference  
15 generation circuit for increasing or decreasing a reference frequency based upon the comparison  
result and a symbol timing circuit, defining consecutive symbol occurrence intervals, in operative  
response to the reference frequency. The symbol timing circuit operates at a sample frequency  
having an integer relationship to the pilot signal. The pilot signal will appear at a correct location  
in the spectrum if the sampling frequency is correct. The pilot signal will be shifted away from  
20 its expected frequency location, in a first direction, if the sampling frequency is too high, and will  
be shifted away from the expected frequency location, in the other direction, if the sampling  
frequency is too low.

The equivalent filter passband signals, containing an augmented pilot, are provided as  
inputs not only to a symbol timing loop, but also to first and second carrier recovery loops.  
25 Carrier recovery and symbol timing is therefore performed in operative response to the same  
augmented pilot input signal.

Carrier phase tracking is decision directed and is performed by circuitry which is  
incorporated into a receiver's adaptive equalizer section. Carrier phase tracking is performed on  
symbols modulated in accordance with both QAM and VAB modulation schemes, and  
30 particularly in the case where VSB signals are treated as OQAM. Treating a VSB signal as  
OQAM allows for carrier phase tracking systems to evaluate both a symbol's error magnitude  
characteristic, but also to evaluate a symbol's rotational state, in order to define a complete phase  
error vector for a VSB (OQAM) signal.

In one aspect of the invention, an integrated circuit digital communication system includes  
35 a decision directed symbol error magnitude determination circuit and a symbol rotation direction  
indication circuit. The symbol error magnitude circuit is operative in response to a first-phase  
portion of a complex signal, while the symbol rotation direction indication circuit is operative  
in response to a second-phase portion of the complex signal, offset from the first-phase portion.

1 The decision directed of symbol error magnitude circuit includes a decision circuit operating on the first-phase signal and outputting first-phase decisions. An error circuit sums the first-phase decisions  
with the first-phase signal in order to define first-phase error term. The symbol rotation direction  
5 indication circuit includes a multiplier which combines the first-phase error term with a signal representing a second-phase midpoint signal.

In a further aspect of the invention, an integrated circuit digital communication system includes a decision directed carrier phase recovery circuit for complex signals representing symbols, characterized by in-phase and quadrature-phase portions separated, in time, by an  
10 offset. The carrier phase recovery circuit includes a sampling circuit of which samples each of the in-phase and quadrature-phase portions of the complex signal at the in-phase and quadrature-phase sampling times. The signal on each rail is thus sampled twice, once at its symbol sampling time and once at its symbol midpoint time.

A separation circuit separates the sampled in-phase (I) signal into a (I) sample time data  
15 stream and an in-phase time offset ( $X_I$ ) data stream, with ( $X_I$ ) being the I midpoint. When both I and Q signals are present, as in the OQAM case, the Q signals are separated into a Q sample time data stream and a  $X_Q$  offset data stream, with  $X_Q$  representing the Q midpoint. The  $X_Q$  and I signals therefore have the same time stamp, as do the  $X_I$  and Q signals. A decision circuit receives the I data stream and generates a tentative symbolic decision from I sample data. The  
20 summing circuit combines the symbolic I decisions with signals from the I data stream in order to generate a I symbolic error term ( $E_I$ ). A multiplier combines the  $E_I$  error term with either  $X_Q$ , or the sign of  $X_Q$  in order to define a phase error term  $P_I$  representing both the error magnitude and rotation direction of symbols on the I rail. Magnitude and direction are, thus, determined from complex signal representations having the same time stamp.

25 In a further aspect of the invention, the integrated circuit digital communication stream includes a second separation circuit connected to separate sampled Q signals into a Q sample time data stream and a  $X_Q$  time offset data stream. A second decision circuit receives the Q sample time data stream and generates a tentative Q symbolic decision from Q sample data. The  
30 second summing circuit combines the tentative Q symbolic decisions with signals from the Q sample time data stream in order to generate a Q symbolic error term ( $E_Q$ ). The second multiplier circuit combines  $E_Q$  with  $X_I$  in order to define a phase error term  $P_Q$  for signals on the Q rail.  $P_I$  and  $P_Q$  signals are sequentially provided by a multiplexer to a loop filter and then to a reference synthesizer circuit which provides phase correction signals to a de-rotator, an operative response to the phase error terms.

35 In yet a further aspect of the invention, where no signals are present on the Q rail, the system receives I signals and takes their Hilbert transform in a Hilbert transform circuit, in order to internally generate a  $X_Q$  signal. A decision circuit makes a tentative symbolic decision on I and a summing circuit combines the tentative decision with I in order to generate an error term

1  $E_1$ . The error term  $E_1$  is combined with the Hilbert transform of  $I$ , i.e.,  $X_Q$ , in order to define a  
phase error term  $P_1$  of which is, in term, directed to a loop filter and reference synthesizer circuit  
for providing phase correction signals to a de-rotator. The error term  $E_1$  is directed through a  
5 delay matching circuit, constructed to provide an identical delay to the  $E_1$  term as the Hilbert  
transform circuit provides on its signal path. Accordingly,  $E_1$  and  $X_Q$  signals arrive substantially  
simultaneously at a multiplier for combination into a  $P_1$  phase error term.

The present invention is further directed to reducing the input wordlength of a decision  
feedback filter, thereby linearly reducing the complexity of a decision feedback equalizer.

10 In a first aspect of the invention, an integrated circuit digital communication system  
includes a decision feedback equalizer, capable of operating on 256-QAM symbols. 256-QAM  
symbols require 8-bits for representation of the symbols at the input to a decision feedback filter.  
These are further divided into 4-bits representing real symbols and 4-bits representing imaginary  
symbols. Utilizing a two's compliment numbering system for implementing signal processing  
functions results in a  $-1/2$  bit offset in the representation of the QAM symbols.

15 An integrated circuit receiver includes an adaptive decision feedback equalizer which  
comprises a feedforward filter, a decision circuit and a decision feedback filter, coupled in  
parallel fashion with the decision circuit. An offset generation circuit provides an offset signal  
which is summed with the output signal from the decision feedback filter. The offset signal  
corresponds to a bitwise representation of a fixed DC offset component resulting from two's  
20 compliment representation of a symbol.

In a particular aspect of the invention, each symbol might be represented with a 4-bit  
representation in two's compliment. This results in a representation which is incorrect by a fixed  
offset equal to  $-1/16$ , which can be corrected by adding a fifth bit to each symbol's representation.  
A decision feedback filter is constructed to receive a symbol decision from a slicer, for example,  
25 having a wordlength of 4-bits, the decision feedback filter outputting a compensated symbol  
decision having a wordlength of 4-bits. An offset generation circuit generates a DC value  
corresponding to the fifth bit representation, and a summing circuit combines the decision  
feedback filter output with the DC value generated by the offset generation circuit. The decision  
feedback filter convolves a 4-bit wordlength symbol decision with adaptively developed  
30 coefficients, while the offset generation circuit convolves the DC value with a set of filter  
coefficients received from the decision feedback filter. The summing circuit, thus provides a full  
ISI compensation signal corresponding to a full 5-bit symbol representation.

In a further aspect of the invention, in the case where the receiver receives VSB  
transmissions utilizing a pilot tone as a carrier reference, the DC component representing the  
35 pilot tone is further convolved with a set of coefficients received from the decision feedback  
filter, in order to develop a compensation signal representing a previously extracted DC  
component.

In accordance with practice of the invention, a method for adaptively equalizing symbols,

1 expressed as digital words, might be characterized as identifying a nibble component of the word,  
where the nibble component represents a particular fixed offset value. The word is truncated to  
a vestigial representation which excludes the nibble component. The vestigial representation is  
convolved with coefficient tap value in a decision feedback filter while the fixed offset value,  
5 corresponding to the excluded nibble component, is convolved with the same coefficient tap  
values in a correction filter. The complexity of circuitry used to implement the decision feedback  
filter is thereby linearly reduced, with a corresponding minimal increase in integrated circuit  
hardware represented by the correction filter.

The present invention is also directed to digital data communication systems and methods  
10 for operating such systems in order to improve the system's bit error rate in high noise situations.  
Decision directed adapted equalization, decision directed carrier and/or timing recovery loops  
are all able to recover significant performance improvements by employing maximum likelihood  
sequence estimation circuitry to provide a higher percentage of correct symbolic decisions. In  
particular, such systems are particularly beneficial in the case of U.S. Digital Terrestrial  
15 Television Broadcasting applications which employ a trellis coded 8-VSB modulation scheme.

In one aspect of the invention, an integrated circuit receiver includes decision directed  
carrier and timing recovery circuits and further includes a decision feedback equalizer. The  
decision feedback equalizer is constructed with a feedforward filter and a decision feedback filter  
and incorporates a trellis decoder circuit, coupled to receive symbol samples from the  
20 feedforward filter and channel perturbation compensation signals from the decision feedback  
filter. The trellis decoder circuit is also integrated into the timing loops so as to provide enhanced  
reliability symbolic decisions to an input of the timing loops.

The trellis decoder includes a decision device, a path metrics module which defines and  
stores path metrics for a sequential series of symbolic decisions, and a traceback memory module  
25 which stores best survivor paths for a sequential series of symbolic decisions. The traceback  
memory has a length N, the Nth decision representing a final decision and the length N represents  
a N stage trellis defined path memory, each stage having a time delay characterized by  $1/N$ . A  
summing circuit is coupled in parallel fashion across the trellis decoder. The summing circuit  
combines an input symbol, input to the trellis decoder, with a symbolic decision, output from the  
30 trellis decoder, to define a sequence estimated error term. A variable delay stage is coupled to  
delay the input symbol by an amount equal to the delay introduced to an output decision by an  
action of the trellis decoder.

In a further aspect of the invention, the feedforward filter includes adaptively updateable  
coefficient taps. The decision feedback filter further includes adaptively updateable coefficient  
35 taps. The sequence estimated error term is provided to the feedforward filter and to the decision  
feedback filter in order to drive the tap updates in a more error free manner.

Increased performance and reliability of both the decision feedback equalizer and timing  
recovery loops are further achieved by optimizing the tradeoff between trellis decoder symbolic

1 decision delay and symbolic decision reliability. In particular, using decisions closer to the Nth  
decision increases the reliability of a particular decision. However, increasing delay in a timing  
recovery loop, by using a symbolic decision closer to the Nth decision, reduces the loop's  
bandwidth and tracking ability. Accordingly, various intermediate symbolic decisions, less than  
5 the Nth decision, are selectively provided to the various timing recovery loops in order to recover  
some degree of sequence estimated decision performance with a minimum of delay consequence.  
Other intermediate symbolic decisions, or a final symbolic decision, is provided to the DFE in  
order to maximize performance.

One particular aspect of the present invention might be implemented in a dual mode  
10 QAM/VSB receiver system such as illustrated in simplified, semi-schematic block diagram form  
in FIG. 1. The receiver system illustrated in FIG. 1 can be described as a digital receiver which  
is compatible with both North American digital cable television and digital terrestrial broadcast  
television standards. The receiver system of FIG. 1 is capable of receiving all standard-definition  
and high-definition digital television formats (SDTV/HDTV).

15 In accordance with principles of the invention, the receiver system depicted in FIG. 1  
accepts an analog signal centered at standard television IF frequencies, amplifies and digitizes  
the input analog signal with an integrated programmable gain amplifier and 10-bit A/D converter.  
Digitized signals are demodulated and filtered with a combined 64/256-QAM and 8/16-VSB  
demodulator and are adaptively filtered to remove multipath propagation effects and NTSC co-  
20 channel interference. The resulting digital data is error corrected with integrated trellis and Reid-  
Solomon decoders which support both the ATSC A/53 and ITU T J.83 Annex A/B/C coding  
formats. The final receive data stream is delivered in either parallel or serial MPEG-2 transport  
format for displaying on a television screen. It should be noted that the receiver system of FIG.  
1 is suitable for digital CATV/HDTV set-top box applications as well as digital CATV/HDTV  
25 televisions.

In the exemplary embodiment of the receiver of FIG. 1, all clock, carrier, gain acquisition  
and tracking loops are integrated with the demodulation and decoding functionality on a single  
integrated circuit chip, as are the necessary phase-locked-loops, referenced to a single external  
crystal.

30 The analog front end of the dual mode QAM/VSB receiver of FIG. 1, indicated generally  
at 10, suitably includes a programmable gain amplifier (PGA) 12 and a 10-bit analog-to-digital  
(A/D) converter 14. The PGA 12 is controlled by an on-chip gain recovery loop, operating in  
conventional fashion, to implement an automatic gain control (AGC) function. The A/D  
converter 14 is clocked by an on-chip voltage controlled oscillator (VCO) which is locked to an  
35 off-chip crystal resonator functioning as a stable timing reference. This stable reference allows  
an input intermediate frequency (IF) signal to be subsampled in order to produce a digital data  
stream centered on a substantially lower IF center frequency.

1 Digressing momentarily, it should be noted that the dual mode QAM/VSB receiver of FIG.  
1 contemplates supporting two modes of IF input signals, direct sampling of a QAM spectrum  
centered on a low IF, or subsampling of a QAM spectrum centered on a standard tuner IF  
frequency of 44 Megahertz (MHz). In low IF mode, the output of a conventional tuner is first  
5 passed through a 6 MHz SAW filter centered on the tuner IF frequency to limit out-of-band  
signal energy. The differential SAW output is then AC coupled to a conventional  
downconversion circuit which centers the QAM spectrum on a low IF such as 6 MHz, and  
amplifies it under control of the AGC 12 to provide a nominal 1.0 volt peak-to-peak signal.

Returning now to the exemplary embodiment of FIG. 1, the dual mode QAM/VSB  
10 receiver according to the invention further includes an IF DC offset cancellation circuit 16 which  
compensates for any DC shift introduced by the A/D circuit 14. A complex mixer (also termed  
a derotator) 18 subsequently converts IF sample data into baseband data and is controlled by a  
direct digital frequency synthesizer (DDFS) driven by the carrier frequency recovery loop in a  
manner to be described in greater detail below.

15 The QAM/VSB receiver's demodulator section suitably incorporates the complex digital  
mixer 18 and a multi-rate filter/interpolator (HB/VID) 20 which in combination, converts an over  
sampled IF input signal to a baseband complex data stream which is correctly sampled in both  
frequency and phase, under control of a clock recovery loop, in a manner to be described in  
greater detail below.

20 In-phase (I) and quadrature phase (Q) baseband signals are then filtered by square-root  
Nyquist filters 22 which can accommodate roll-off factors of 11-18%. The outputs of the square-  
root Nyquist filters are subsequently directed to an adaptive equalization block 24 and are  
parallel-processed by a Nyquist-type prefilter 26 to provide an input signal to an  
acquisition/tracking loop circuit 28 which includes carrier recovery loop circuitry to support  
25 carrier frequency recovery and spectrum centering as well as baud recovery loop circuitry, for  
symbol timing extraction, as will be described in greater detail below.

Prior to being directed to the Nyquist prefilter 26 and adaptive equalization block 24,  
filtered signals are provided from the square-root Nyquist filter 22 to an NTSC co-channel  
interference rejection filter 28, for removal of the luma, chroma, and audio subcarrier signals  
30 from the frequency spectrum. When used in a terrestrial environment, there exists the possibility  
of co-channel interference from terrestrial-type NTSC transmitters. The NTSC co-channel  
rejection filters 28 function as an adaptive digital filter which places precisely located notches  
in the frequency spectrum at the specific locations of the NTSC luma, chroma, and audio  
subcarriers. An NTSC co-channel rejection filter suitable for implementation in connection with  
35 the dual mode QAM/VSB receiver system of FIG. 1, might be one such as described in co-  
pending patent application serial No. 09/303,783, filed, May, 11, 1999 and entitled "NTSC  
REJECTION FILTER", commonly owned by the Assignee of the present invention, the entire  
disclosure of which is expressly incorporated herein by reference.



1 While the square-root Nyquist filters 28 ordinarily assure that there is a minimal inter-  
symbol interference (ISI) over a perfect channel, the Nyquist filters are unable to remove ISI due  
to the imperfect channel characteristics. Accordingly, the dual mode QAM/VSF receiver  
according to the invention, provides an adaptive, multi-tap decision directed equalizer circuit 24,  
5 having 64 feedforward taps and 432 feedback taps, which is sufficient to remove ISI components  
generated by worst-case coaxial cable and terrestrial broadcast channels with multi-path spreads  
of up to 40  $\mu$ sec at 10.76 Mbaud.

Blind convergence algorithms are utilized by the equalizer 24 along with an ability to  
implement a training sequence embedded in the incoming data stream. In addition to adaptive  
10 equalization, the decision directed equalizer 24 also includes particular circuitry to perform  
carrier frequency acquisition and phase tracking (in the case of QAM modulation) or carrier  
phase tracking (phase recovery in the case of VSB modulation) on equalized constellation points  
using a quadrature synthesizer and complex mixer under control of the carrier recovery loop, to  
track out residual carrier offsets and instantaneous phase offsets such as are caused by tuner  
15 microphonics, as will be described in greater detail below.

The dual mode QAM/VSF receiver exemplified in FIG. 1 further includes a forward error  
correction (FEC) and decoder block 32, which is compatible with all common CATV standards  
and the ATSC terrestrial broadcast standard. Specifically, the Annex A/C decoder circuitry  
implements four general functions, frame synchronization, convolutional deinterleaving, reed-  
20 Solomon error correction and derandomization. Hard decisions are input to the frame  
synchronizer which locks onto the inverted synch byte pattern, conventionally provided in  
television data frames. After synchronization, data interleaving is removed by a convolutional  
deinterleaver utilizing a Ramsey type III approach. Data symbols are next provided to a Reed-  
Solomon decoder, which is able to correct up to 8 symbol errors per RS block, followed by data  
25 derandomization to undo the corresponding randomization operation of the transmitter's  
modulator.

In the Annex B mode, the decoder typically performs five general functions, and differs  
from the Annex A/C case primarily in its use of trellis decoding. Soft decisions from the  
receiver's equalizer circuit are input to a trellis decoder which functions as a maximum likelihood  
30 sequence estimator. Output sequences are directed to a frame synchronizer and derandomization  
block, similar to those described above, in connection with Annex A/C decoding. Data then is  
directed to a Reed-Solomon decoder block which is capable of correcting 3 symbol errors per RS  
block. A checksum decoder identifies blocks with uncorrectable errors and flags an output  
MPEG-2 data stream with a Transport Error Indicator (TEI) flag.

35 In practice, the majority of communication with the dual mode QAM/VSF receiver 10 of  
FIG. 1, and the majority of the activity provided by the various functional blocks, takes place  
upon initiation of a channel change. Upon detection of a channel change request, a receiver  
system's host microprocessor determines whether the existing 6 MHz channel contains the

1 requested MPEG service or if another channel must be selected. In the latter case, the host  
microprocessor typically consults its program table and might direct the receiver system to  
program a channel tuner to select the appropriate channel frequency. The host microprocessor  
might then download, to the receiver 10, any channel specific configuration that might be  
5 required, such as the configuration of the receiver and FEC 32 for reception of either a terrestrial  
(VSB) or a cable (QAM) channel.

Following configuration download the receiver 10 must acquire lock, i.e. synchronize its  
acquisition and tracking loop circuitry 30 to the frequency and phase of a remote transmitter.  
Receiver lock is a multi-step process which generally involves allowing the various  
10 acquisitions/tracking loops to acquire lock in a predetermined manner. For example, the AGC  
loops are generally allowed to acquire first, in order to ensure that the signal level at the input to  
the A/D converter 14 is set appropriately. AGC bandwidths are initially set wide open in order  
to minimize acquisition time and subsequently reduced to provide adequate tracking and minimal  
noise.

15 Carrier frequency acquisition and symbol timing (baud timing) are typically enabled after  
the AGC loops have acquired lock. Depending on the particular mode of operation (QAM or  
VSB), these may be obtained jointly or in sequence. In a manner to be described in greater detail  
below, each loop is allowed to acquire by widening the appropriate bandwidths, thus allowing  
the loops to pull-in the signal, and gradually reducing the bandwidth as lock is obtained. Once  
20 baud timing and carrier frequency is acquired, a carrier phase loop is enabled. While the carrier  
frequency loop is typically able to obtain a coarse phase lock, its ability to track instantaneous  
phase noise is compromised. A carrier phase loop provides a superior ability to track out phase  
noise.

Once the receiver system 10 has obtained lock, recovered data is delivered to the FEC  
25 decoder 32. The FEC 32 first obtains node synchronization (if there is a trellis decoder in the  
selected coding scheme), following by frame synchronization. With frame synchronization  
achieved, derandomization and deinterleaving are performed along with Reed-Solomon decoding.  
MPEG-2 transport stream synchronization is then achieved and data is delivered to the output  
for display.

30 The carrier frequency/phase recovery and tracking loops are all-digital loops which  
simultaneously offer a wide acquisition range and a large phase noise tracking ability. In  
accordance with the present invention, the loops use both pilot tracking and decision directed  
techniques in order to estimate the angle and direction for phase/frequency compensation. The  
loops are filtered by integral-plus-proportional filters, in which the integrator and linear  
35 coefficients of the filter are programmable to provide means for setting loop bandwidths. The  
baud recovery loop includes a timing error discriminant a loop filter, and digital timing recovery  
block which controls a digital resampler. As was the case with the carrier loops, the baud loop's  
timing error discriminant outputs a new value each baud which is filtered by a digital integral-

1 plus-proportional filter featuring programmable coefficients.

In accordance with the present invention, the dual mode QAM/VSF receiver system 10 of FIG. 1 is configurable to be operable with both North American digital cable television (QAM) and digital terrestrial broadcast television (VSF) standards as well as performing in a dual  
5 QAM/VSF mode, it should further be understood that VSF broadcasts might be one of two separate types, a first, terrestrial broadcast mode (referred to as 8 VSF) which supports a payload data rate of about 19.28 Mbps in a 6 MHz channel, and a second, high data rate mode (referred to as 16 VSF) which supports a payload data rate of about 38.57 Mbps. Both of these modes are well understood and described in the ATSC digital television standard, put forth by the advanced  
10 television systems committee. VSF transmission inherently requires only processing an in-phase (I) channel signal which is sampled at the symbol rate. In contrast, QAM transmission requires that the receiver process both in-phase (I) channel signals and quadrature-phase (Q) channel signals which are sampled at its symbol rate, typically one half that of a comparable VSM.

A comparison of the spectral distribution of QAM modulated signals and VSF modulated signals is illustrated in FIG. 2. Each of the spectra, for the QAM and VSF cases, are subtended  
15 by an

"eye" diagram illustrating the signal content for both the I and Q rails. Although the VSF spectrum might be viewed as the sum of a real spectrum and its Hilbert transform, the VSF spectrum might further be considered as a frequency shifted Offset-QAM (OQAM) spectrum. Accordingly, the dual mode QAM/VSF receiver 10 of FIG. 1 is configured, when in VSF mode,  
20 to treat VSF modulated signals as either VSF or as OQAM, depending on the desires of the system configuration engineers.

FIG. 2 includes an Offset-QAM spectrum subtended by its corresponding "eye" diagram, in which the distinctive feature of OQAM is evident. In particular, signals on the Q rail are delayed by one half of a symbol, thus offsetting the Q rail, in time, from information on the I rail.  
25 As can be seen in the VSF and OQAM spectra of FIG. 2, and as more particularly evident in the VSF channel occupancy diagram of FIG. 3, the spectrum occupying a nominal 6.0 MHz channel is generally flat, except for symmetrical band edge regions where a nominal square root raised cosine response results in 620 kHz transition regions 36 and 38.

The dual mode QAM/VSF receiver in accordance with the invention is capable of operating on transmitted signals modulated by any of the above modulation formats with substantially the same circuitry. Particularly, and where appropriate, the receiver treats VSF modulated signals as though they were OQAM because of the frequency shift relationship therebetween. Where signals are required to be treated as VSF signals, processing blocks include  
30 a real to imaginary converter circuit, in particular a Hilbert transform filter, which creates an analogue Q rail signal from the VSF real I rail, in order to use complex circuitry which directly extracts an error vector quantity.

1       Where a VSB signal is considered an OQAM signal, processing blocks include a time  
compensation circuit, such as a  $Z^{-1/2}$  transform circuit, in order to accommodate the one half  
symbol delay inherent in an OQAM symbol period (and VSB symbol period) with respect to a  
QAM symbol period. Time compensating the Q rail of an OQAM signal allows the system to  
5       accommodate the sampling rate  $F_s/2$  of VSB to the sampling rate  $F_s$  of QAM. In addition, when  
a VSB signal is demodulated as OQAM, the received VSB spectrum is mixed to "baseband at the  
spectrum's center frequency and the received complex data stream can be viewed as similar to  
QAM with a one half symbol offset between the in-phase and quadrature-phase components. The  
effective "symbol rate" of the VSB signal is thereby halved, making it substantially similar to  
10       QAM symbol rates and allowing interchangeability of receiver component processing blocks.

A pilot signal 40, typically a 50 kHz pilot signal, is added to the spectrum by a pilot  
insertion circuit, implemented in accordance with the standard, in all transmitters. The pilot  
signal 40 is typically provided at a spectral position, 310 kHz from the lower band edge, that was  
reserved for the suppressed carrier signal in conventional NTSC transmissions. This suppressed  
15       carrier signal provided a frequency reference signal to which NTSC receivers could lock and  
which was used for carrier recovery. The pilot is also termed "pilot tone" and (misleadingly)  
"carrier".

Carrier recovery is conventionally performed by an FPLL synchronous detector, which  
integrally contains both the frequency loop and a phase-locked loop in one circuit. The frequency  
20       loop provides wide frequency pull-in range of approximately  $\pm 100$  kHz while the phase-locked  
loop might be implemented with a narrower bandwidth, i.e., typically less than 2 kHz. Further,  
in the ATSC digital television standard, the recommended approach to recover symbol timing  
information is to utilize a data segment sync signal that makes up a VSB data segment, and which  
is inserted between every segment of 828 symbols. The repetitive data segment sync signals are  
25       detected from among synchronously detected random data by a narrow bandwidth filter. From  
the data segment sync signals, a properly phased 10.76 MHz symbol clock is conventionally  
created.

In accordance with the present invention, the dual mode QAM/VSB receiver 10 of FIG.  
1 recovers timing information from the pilot (unsuppressed carrier) signal that is included with  
30       the VSB signal, whereas the ATSC specification intends that the pilot signal be used only for  
carrier recovery.

Turning now to FIG. 4, there is depicted in simplified, semi-schematic block diagram  
form, an exemplary embodiment of a unitary carrier and recovery and symbol timing loop  
architecture, termed "unitary" in that both functions, frequency acquisition and tracking and  
symbol timing (also termed "baud recovery") are operable in response to the pilot (unsuppressed  
35       carrier) signal. In the embodiment of FIG. 4, an input IF spectrum is digitized by an analog-to-  
digital converter (A/D) and the resulting digital complex signal is directed to a complex mixer  
50 where it is combined with a complex signal having a characteristic frequency  $f_c$  equal to the

1 carrier frequency. The resulting complex signal is processed by a highband filter and variable  
rate interpolator, represented as a single processing block in the embodiment of FIG. 4, and  
denoted HB/VID 52. In a manner to be described in greater detail below, symbol timing is  
performed by a baud loop coupled to provide symbol timing information to the variable rate  
5 interpolator (VID) portion of the HB/VID filter 52. Following interpolation, baseband IF signals  
are processed by a square root Nyquist filter which has a programmable roll off  $\alpha$  of from about  
11 to about 18%. The square root Nyquist filter 54 is further designed to have a particular cutoff  
frequency that has a specific relationship to the VSB pilot frequency  $f_c$ , when the VSB spectrum  
centers at DC. In a manner to be described in greater detail below, this particular cutoff  
10 frequency is chosen to have this particular relationship in order that both carrier recovery and  
symbol timing recovery might be based on a VSB pilot frequency enhancement methodology.

An NTSC rejection filter 56 is provided in the signal path in order that interference  
components represented by the luma, chroma and audio subcarriers, present in NTSC terrestrial  
broadcast system signals, are removed from the digital data stream prior to the data being directed  
15 to the receiver system's equalizer. The NTSC rejection filter 56 is an all digital, programmable  
notch filter, exhibiting quite narrow notches at specific, predetermined frequencies that  
correspond to the luma, chroma and audio subcarrier peaks. Although the NTSC rejection filter  
56 is contemplated as functioning to remove unwanted NTSC co-channel interference  
components, the characteristics and design of the NTSC rejection filter 56 are such that it may  
20 be used to remove any form of interference component having a deterministic relationship to a  
particular input spectrum.

Following the filter bank, the input baseband signal is directed to a second mixer 58 where  
it's combined with a correction signal, developed in a manner to be described in greater detail  
below, which ensures that the spectrum is appropriately centered about zero.

25 It will thus be understood that there are two stages to carrier acquisition, a first stage,  
termed "an outside stage" (or outside loop) provides for mixing the received digitized spectrum  
down to baseband and which might properly be termed "a tracking loop", and a second correction  
stage, termed "an inside loop", which functions more as an acquisition loop and which provides  
a correction factor to the spectrum to make sure the spectrum is properly centered. In addition,  
30 the correction factor is "leaked" from the inside loop to the outside loop in order that the inside  
loop might be constructed with a wide bandwidth, typically in the 100 kHz range in order to  
provide for fast acquisition. Correction factors are leaked to the outside loop such that the  
outside loop might be constructed with a relatively narrow bandwidth in order to provide for  
more accurate tracking capability. Once the carrier has been acquired.

35 A carrier phase detector 60 is coupled to receive an input signal from a Nyquist prefilter  
62 coupled in turn to receive complex signal from a node between the second mixer 58 and the  
receiver's equalizer 64. The Nyquist prefilter 62 is constructed as a high pass filter with a cutoff  
at the same particular characteristic frequency as the cutoff designated for the low pass root

1 Nyquist filter 54. The root Nyquist filter 54 and Nyquist prefilter 62 function in combination to  
define an equivalent filter that acts to define the pilot enhanced timing recovery characteristics  
of the receiver in accordance with the present invention. Complex, pre-filtered signals are  
directed to the input of the carrier phase detector which produces a 6-bit frequency error  
5 discriminant for use in the loop. The SGN function of these 6-bits are extracted and applied,  
simultaneously, to an inside loop filter 66 and an outside loop filter 68. The inside loop filter 66  
drives an inside timing reference circuit, such as a direct digital frequency synthesizer (DDFS)  
which might also be implemented as a voltage controlled oscillator (VCO) or a numerically  
controlled oscillator (NCO). Likewise, the outside loop filter 68 drives an outside timing  
10 reference circuit 72 which might also be suitably implemented as a DDFS, VCO, or an NCO.  
As was mentioned previously, the outside, or centering, loop functions to define a complex signal  
that might be expressed as  $\sin \Omega_c$  and  $\cos \Omega_c$ , where  $\Omega_c$  represents the pilot (carrier) frequency.  
Since the pilot (carrier) frequency  $f_c$  is given, its position in the frequency domain, with respect  
to any sampling frequency  $f_s$  is deterministic. Therefore, if a receiver system wishes to lock its  
15 timing frequency to a particular  $F_s$  that has a fixed relationship with a known  $F_c$ , as in the case  
of the ATSC standard signals, it need only apply a phase lock loop that tracks the pilot.  
Axiomatically, the pilot signal will appear at the correct location in the spectrum if the sampling  
frequency  $F_s$  is correct. The pilot signal will be shifted to a lower frequency from its expected  
frequency location if the sampling frequency  $f_s$  is too high. Conversely, in the case where the  
20 sampling frequency  $f_s$  is too low, the pilot signal will appear to have been shifted to a higher  
frequency location from its expected frequency location in the spectrum.

A particular case which makes implementation of pilot enhanced carrier recovery simpler,  
occurs when the sampling frequency  $f_s$  is selected to be four times that of the pilot frequency  $f_c$ ,  
when a VSB spectrum is centered at zero. Thus, when the spectrum is centered, the pilot signal  
25 will be expected to occur at  $f_c$ . In accordance with practice of the present invention, the inside  
and outside loops will be looking for the pilot to occur at a frequency of  $f_s/4$ . This particular  
implementation is illustrated in the semi-schematic block diagram of FIG. 5 and its  
corresponding spectrum diagrams of FIG. 6.

As mentioned previously, the receiver system incorporates a frequency modulated square  
30 root Nyquist low pass filter 54 in combination with a high pass Nyquist prefilter 62, which in  
combination might be viewed as a single equivalent filter 74. Both the root Nyquist 54 and  
Nyquist prefilter 62 are constructed with cutoff frequencies of  $f_s/4$ . Thus, and as indicated in the  
spectrum diagrams of FIG. 6, the high pass Nyquist prefilter 62 gives a resultant high and low  
band spectrum with each centered about  $F_s/2$ . When the spectra of the root Nyquist filter 54 and  
35 Nyquist prefilter 62 are superposed (summed as would be the case with an equivalent filter 74)  
the resultant signal is a symmetrical waveform, centered at  $F_s/4$ , each of which are centered about  
and symmetric with respect to the pilot when the pilot frequency  $f_c$  is equal to  $f_s/4$ . Accordingly,  
since the pilot signal is designed to be centered within a spectrum's transition band, the

1 combination of the root Nyquist filter 54 and Nyquist prefilter 62 define an equivalent filter 74  
that provides an output signal symmetric about the pilot when the pilot (carrier) has been  
appropriately acquired. It will thus be understood that when the equivalent filter output is  
symmetric about the pilot  $f_c$ , the resulting waveform can be represented as a pure sinusoidal  
5 signal for which only zero crossings need to be evaluated by the carrier phase detector (60 of  
FIG.4). If the sampling frequency  $f_s$  is too high, not only will the pilot signal be observed to  
appear at a lower frequency than its expected frequency location, but also the symmetry of the  
resultant waveform from the "equivalent" filter 74 will also be disturbed due to the non-center  
placement of pilot. Likewise, when the sampling frequency  $f_s$  is too low, the pilot signal will be  
10 observed to appear at a higher frequency than its expected frequency location, also perturbing the  
symmetry of the equivalent filter's output in a direction opposite the previous case. The carrier  
phase detector (60 of FIG. 4) evaluates the position of the pilot with respect to the sampling  
frequency and provides appropriate correction signals to the inside loop filter (66 of FIG. 4) and  
the outside loop filter (68 of FIG. 4).

15 During initialization, one is able to make certain assumptions about the pilot signal since  
its frequency  $f_c$  position with respect to the spectrum is deterministic. Accordingly, while the  
inside or acquisition, loop is acquiring the pilot, the outside, or centering, loop assumes that no  
frequency offset has been introduced to the spectrum and runs the DDFS (or VCO, or NCO) in  
a "flywheel" mode. Since the IF input signal is centered at 6 MHz, the outside timing reference  
20 (72 of FIG. 4) also runs at 6 MHz until such time as the inside loop is able to acquire the carrier  
and "leak" any frequency offset information so obtained to the outside loop filter (68 of FIG. 4)  
for developing appropriate control signals for the outside loop's timing reference (72 of FIG. 4).

Returning now to FIG. 4, the Nyquist prefilter 62 further provides a complex input signal  
to a baud loop (also termed "symbol timing loop") which provides symbol timing information  
25 to the variable rate interpolator 52. The baud loop suitably includes a baud phase detector circuit  
76 coupled, in turn, to a baud loop filter 78 which controls operation of a baud timing generation  
circuit 80 such as a DDFS, VCO or NCO.

A further implementation of a baud loop is illustrated in the simplified semi-schematic top  
level block diagram of FIG. 7. The implementation of the baud loop depicted in FIG. 7 is  
30 generally similar to that depicted in the acquisition and tracking loop diagram of FIG. 4, and  
suitably includes a baud phase detector coupled to receive complex signals  $I_{pref}$  and  $Q_{pref}$   
from the Nyquist prefilter. The baud phase detector 76 might be implemented as a timing error  
discriminant which outputs a new value each baud, in turn, filtered by a digital integral-plus-  
proportional low pass filter 78. The filtered signal is summed at a summing node 80 with an  
35 offset word, denoted "baud frequency control word" or SCW, and is used to control operation  
of a baud numerically controlled oscillator (NCO) 82. The loop is updated once per baud, but  
only if a sine change occurred on either the I or Q decision data since the previous baud. The  
summing node 80 and frequency control word are provided in order to accommodate the baud

1 loop to any known offsets that might, for example, have been acquired from past history of communication between the receiver and a particular remote transmitter unit.

FIG. 8 is a semi-schematic block diagram of an exemplary implementation of the baud phase detector 76 of FIG. 7. In the exemplary embodiment of a baud phase detector of FIG. 8, the input to the baud loop is the complex signal output by the Nyquist prefilter, I<sub>pref</sub> and Q<sub>pref</sub>. The signal from the I rail might either be offset by one symbol period through a delay element 90 or alternatively, be provided directly to the remaining circuit elements of the baud phase detector through a selection MUX 92. In the case where the baud phase detector is processing a VSB signal, one symbol delay is added for signals on the I rail. In the case where the baud phase detector is processing QAM signals, there is no need to add a symbol delay for either of the I or the Q rail, since the I and Q components of a symbol are aligned within a symbol period. It should also be noted that when VSB signals are being processed as OQAM, a one symbol delay is added to the signals on the I rail by passing the I signals through the delay element 90. Delay selection is made by the MUX 92 in response to a QAM/OQAM (VSB) signal provided by an off-board control microprocessor.

After input, the sign of the symbols on the I and Q rails is determined by a first sign logic circuit 94. The sign of the input symbols is mixed in mixer 104 with the output of a second sign logic circuit 102 which determines the sign of signals appearing on the I Q rails after they have been directed through two sequential delay elements 96 and 98. A third sign logic circuit 100 disposed between the two delay elements 96 and 98 provides an output signal to a second mixer 106 where it is combined with the output of the first mixer 104. The output of the second mixer 106, for both the I and Q signal paths, is summed by a summing circuit 108 and provided to the baud loop's low pass filter (78 of FIG. 7). It will be understood that the baud loop is updated once per baud, but only if a sign change occurred on either the I or Q decision data since the previous baud. The signs of the two previous symbols are evaluated by sign logic circuitry 100 and 102, while the sign of the present symbol is evaluated by sign logic circuitry 94. For example, if two sequential symbols exhibited particular phase relationships such that they might be characterized as rotated in a positive direction (i.e., having a positive sign), and a subsequent symbol exhibiting a phase rotation in the opposite direction (having a negative sign), the combination of the signs of the first and third symbols would combine in mixer 104 to give a negative, and combined in mixer 106 with the sign of the second symbol to further result in a negative. This result would indicate a transition from the prior symbol's phase relationships and be therefore directed to the loop filter for control of the baud NCO. The timing error discriminant, as represented by the signals output by the summing junction 108, is therefore represented by values of -1, 0 or +1, with 0 representing either of the case where I and Q are aligned in time and in phase, or the case where I and Q are not aligned with one another, regardless of their phase relationship with nominal. In this last case, unlike symbols are not



1 necessarily indicative of baud timing, but rather another form of error which it is not the function of the baud loop to compensate.

Returning momentarily to the simplified architectural illustration of an exemplary embodiment of the dual mode QAM/VSB transceiver of FIG. 1, it will be understood that while  
5 the square root Nyquist filters 22 will assure that there is no intersymbol interference (ISI) over a perfect channel, they are unable to remove ISI components due to imperfect channel characteristics. Accordingly, After the filter block represented by the HB/VID 20, root Nyquist 22 and NTSC 28 filters, the dual mode QAM/VSB receiver provides a decision directed equalizer, incorporating both a feedforward equalizer and decision feedback equalizer for  
10 removing such ISI components. In the exemplary embodiment, the adapted equalizer 24 might be constructed as a 496-tap decision directed equalizer with 64-real/16-complex feedforward (FFE) taps and 432-real/108-complex feedback (DFE) taps, which is sufficient to remove ISI generated by worst-case coaxial cable and terrestrial broadcast channels. In addition to adaptive equalization, the adaptive equalizer 24 also includes circuitry for performing phase recovery on  
15 equalized constellation points, by using a quadrature synthesizer and complex mixer under the control of a carrier recovery loop, in order to track out residual carrier offsets and instantaneous phase offsets such as are caused by tuner microphonics. Further, the adaptive equalizer 24 is implemented such that the same hardware is configurable for either QAM or VSB applications, with a complex implementation being used for QAM and a real implementation being used for  
20 VSB.

In the case of QAM modulated signals, both carrier frequency and phase recovery is performed by circuitry contained within the adaptive equalizer block 24. In the case of VSB modulated signals, the equalizer section further includes circuitry for performing carrier phase recovery. In particular, since the adaptive equalizer incorporates decision directed circuitry, it  
25 is quite amenable to decision directed recovery techniques. For QAM, I and Q are coincident in time, so if I and Q are mixed, both the decision vector and phase offset are directly obtainable.

For VSB (or OQAM), I and Q are offset from one another by one symbol period. Accordingly, some phase rotation metric must be defined before I and Q are directed to the equalizer. As was described above, in connection with FIG. 8, the baud loop artificially puts I  
30 and Q in phase, by action of the initial delay stage (90 of FIG. 8) disposed on the I rail.

Turning now to FIG. 9, there is depicted a simplified, semi-schematic block level diagram of the exemplary dual mode QAM/VSB receiver, including details of the construction and arrangement of adaptive equalizer 24 having decision directed VSB phase tracking and decision directed QAM frequency acquisition and phase tracking loops in accordance with the present  
35 invention. As illustrated in the embodiment of FIG. 9, the adaptive equalizer includes a feedforward (FFE) block 110 configured to receive symbol aligned complex signals centered in baseband. The FFE 110 is suitably constructed as either a 64-tap real FFE, for VSB applications, or a 16-tap complex FFE when used in connection with QAM modulated signals. Carrier phase

1 alignment and/or carrier frequency/phase alignment is performed in a mixer 112 which receives  
signals from the FFE 110 and combines them with a timing reference signal developed by a  
timing reference circuit 114 such as a numerically controlled oscillator (NCO) a voltage  
5 controlled oscillator (VCO) or a direct digital frequency synthesizer (DDDFS). Timed signals  
are then provided to a slicer 116 operating in conjunction with a decision feedback (DFE) block  
118 which, in combination, provide hard decision information on constellation states as well as  
error information relating to differences between actual signal trajectory relative to an ideal signal  
trajectory.

Error signals developed in the equalizer are directed through either a QAM phase detector  
10 120 or a VSB phase detector 122 depending on how the incoming signal has been modulated.  
Choosing between the QAM phase detector 120 and VSB phase detector 122 is a function of a  
multiplex circuit 124 operating in response to a QAM/VSB control signal provided by an off-chip  
microprocessor. A second multiplex circuit 126 couples the output of the QAM phase detector  
120 and VSB phase detector 122 to a low pass filter 128 which, in turn, develops control signals  
15 for the timing reference circuit 114. Thus, the dual mode QAM/VSB receiver can be  
characterized as having four separate and distinct timing loops, operative in various combinations  
depending on whether the incoming signal is VSB or QAM.

In particular, the multiple loop timing system includes a first loop, also termed an inside  
loop, suitably including the Nyquist prefilter 62, carrier phase detector 60, an inside loop filter  
20 66 and an inside timing generation circuit 70 such as an NCO, VCO or DDFS. The inside loop  
functions as a wide bandwidth acquisition loop for frequency recovery on the carrier signal in a  
manner described above. The multiple loop system further includes a second loop, also termed  
the outside loop, which shares the carrier phase detector 60 with the inside loop and which  
functions as a narrow bandwidth centering loop, also for frequency recovery on the pilot signal.  
25 The third loop, of the multiple loop system, is the baud loop which functions to define symbol  
timing. As was described above, the first loop, the inside or acquisition loop, is operative only  
when the received signal is a VSB signal. The fourth loop, of the multi loop system including  
QAM and VSB phase detectors 120 and 122 in combination with Lopez filter 128 and exemplary  
NCO 114, functions as the frequency recovery acquisition loop in the QAM case, as well as the  
30 phase tracking loop for both VSB and QAM cases. As was described in connection with the  
inside and outside loops, above, the phase corrections developed by the QAM phase detector 120  
are "leaked" to the outside loop's loop filter 68 on a 1-bit per period basis so as to provide a  
coarse correction to the outside loop in order that the outside loop can be constructed with a  
narrow bandwidth in order to maintain centering accuracy.

35 In the exemplary carrier recovery loop of FIG. 9, a particular form of phase detection  
employs symbols with the same time stamps for each phase error term, thus allowing acquisition  
and tracking of carrier frequency offset in addition to tracking of carrier phase offset.  
Conventionally, VSB systems use every second consecutive symbol for phase detection, with the

1 two symbols representing one symbol offset. Due to this particular time offset, the resultant carrier loop is insufficient to perform carrier frequency acquisition and tracking, as well as more susceptible to self phase noise, introduced during phase detection when compared to an equivalent QAM phase detection.

5 FIG. 10 is a simplified block diagram of a carrier recovery network such as might be implemented in a dual mode QAM/VSB receiver. The carrier recovery network includes a phase detector 130 configured to receive in-phase I and quadrature-phase Q input signals. The in-phase signal should have been sampled twice a symbol at both the in-phase symbol sampling time and at the quadrature-phase sampling time. The in-phase signal is then 1-to-2 de-multiplexed to  
10 generate two information streams, denoted I and  $X_i$ , where the I represents in-phase symbols sampled at the in-phase sampling time and the  $X_i$  represents mid-symbol points sampled at the quadrature-phase symbol sampling time.

Similarly, the quadrature-phase symbol Q having been sampled twice a symbol is 1-to-2 de-multiplexed to generate two information streams representing the quadrature-phase symbols (Q) and its mid-point symbols ( $X_Q$ ), respectively. Accordingly, when an in-phase signal is de-multiplexed in order to generate a symbol (I), the quadrature-phase signal is de-multiplexed to generate its mid-symbol point ( $X_Q$ ), and *vice versa*

Following de-multiplexing, both the in-phase and quadrature-phase symbols are decoded in respective decision device blocks 136 and 138 to generate symbol decisions I with a 'I' and 'Q', respectively. The original sample value I and Q is arithmetically combined with the decisions 'I' and 'Q' in respective adders 140 and 142 in order to generate an error term  $E_i$  and  $E_Q$ , respectively for the I rail and the Q rail.

Phase error terms are generated, one for each rail, as  $P_i$  and  $P_Q$ , respectively by taking the product of a particular rail's error term and multiplying it by the corresponding rail's mid-symbol point. For example, the phase error term for the I rail,  $P_i$  is equal to the quantity  $(I - 'I') * X_Q$ .

Alternatively, the phase error term  $P_i$  might also be represented as  $(I - 'I') * \text{sign}(X_Q)$ . Similarly, the phase error term for the Q rail can be expressed as  $('Q' - Q) * X_i$ , or  $('Q' - Q) * \text{sign}(X_i)$ . In either case, the I, 'I' and  $X_Q$  in each I rail phase error term computation have the same time index, as do the Q, 'Q' and  $X_i$  for each Q rail phase error term computation. Thus,  
30 there should be a corresponding pair of  $P_i$  and  $P_Q$  phase error terms per symbol which exhibit an offset equal to the offset between the initial I and Q signals.

In accordance with the exemplary embodiment of FIG. 10, each pair of  $P_i$  and  $P_Q$  phase error signals are further multiplexed, in multiplexer 148, in order to generate two consecutive phase error terms, for each symbol, which are provided in turn to a loop filter 150. The loop filter 150 develops control voltage for the loop's VCO 152 which provides a timing reference  
35 signal for an input phase splitter and derotator 154 which functions as a phase correction block.

1       The carrier phase loop of FIG. 10, will be understood to include a phase detector capable of extracting the phase and/or frequency difference between the transmitted carrier and received carrier in order to accurately demodulate received signals.

5       FIG. 11 is a simplified, block level diagram of a carrier phase detection and correction loop as it might be implemented if the receiver were operating in VSB mode. In FIG. 11, the input signal is received by a phase splitter and derotater 154 which provides a single sideband signal (I) to the VSB phase detector 156, along with a counterpart signal  $X_Q$ , where the single sideband signal I and its counterpart  $X_Q$  form a Hilbert transform pair.

10       As was the case in connection with the QAM phase detector 130 of FIG. 10, the I signal is decoded, i.e., quantized to a valid symbol, in a decision device 158 to generate a valid symbol 'I'. The 'I' and the valid symbol 'I' are negatively combined in a summing circuit 160 in order to define an error term  $E_I$ . A multiplier 162 combines the error term  $E_I$  with the sideband signal counterpart  $X_Q$  in order to define a phase error term  $P_I$  which can be expressed as  $(I - 'I') * X_Q$  or alternatively,  $(I - 'I') * \text{sign}(X_Q)$ . The phase error term  $P_I$  is provided to a loop filter 164 which  
15       develops a control voltage for a reference signal synthesizer such as a voltage controlled oscillator (VCO) 166. The synthesized reference is provided, in turn, to the phase splitter and rotater 154 in order to provide a phase correction to incoming single sideband VSB signals.

20       Turning now to FIG. 12, there is depicted a simplified, semi-schematic block diagram of an alternative embodiment of a VSB-type carrier phase detection and correction system in accordance with the present invention. As was the case with the carrier phase detection and correction system of FIG. 11, the system of FIG. 12 receives a single sideband (VSB) signal through a phase splitter and derotater 170 and provides a I signal to a summing junction 172 where it is combined with the output of a decision feedback equalizer (DFE) 174. It should be noted herein that the summing junction 172 and DFE 174 correspond to the summing junction  
25       117 and DFE 118 of the exemplary embodiment illustrated in FIG. 9.

      I rail signals are directed to a decision device 176, such as a slicer, where the incoming I signals are quantized to a valid constellation point 'I'. Quantized symbols, i.e., decisions, are fed back into the DFE 174 and further provided to a second summing junction 178 where they are negatively combined with the input signal I in order to define an error term  $E_I$  representative of  
30       the displacement of the input signal I from its ideal (quantized valid) value. The error signal  $E_I$  may thus be viewed as representing a rotational or phase error of the input signal I from its ideal quantized value 'I'.

      In order to determine the direction of phase rotation, i.e., to determine a phase lead or phase lag, the error  $E_I$  is multiplicatively combined with a midpoint signal  $X_Q$  which is the  
35       Hilbert transform of the input signal I.  $X_Q$  is developed through a Hilbert transform circuit 180.  $X_Q$  might be combined directly with the error term  $E_I$  in a multiplier 182 or alternatively, might be evaluated to determine its sign in an optional sign determination circuit 184. Thus, the output of the exemplary carrier phase detector of FIG. 12 is a generated phase error term  $P_I$  which

1 might be expressed as either  $(I-I') \cdot X_Q$  or  $(I-I') \cdot \text{sign}(X_Q)$ . The phase error term  $P_i$  is directed  
to a loop filter 186 which develops a control signal (a control voltage) that controls the  
operational parameters of a reference signal synthesizer such as a VCO. The synthesized  
reference signal is provided to the phase splitter and derotater 170 which, in turn, "derotates"  
5 incoming signals in order to properly recover and track carrier phase.

It should be understood that the exemplary embodiment of FIG. 12, where the Hilbert  
transform  $X_Q$  of an incoming  $I$  signal is generated internally, is suitably implemented in the case  
where the phase detector is provided in combination with a baseband decision feedback equalizer  
(DFE) or when the derotater is implemented such that only an in-phase component of a received  
10 signal is produced. In the exemplary embodiment of FIG. 11, a Hilbert transform circuit would  
not be required since the Hilbert transform  $X_Q$  of the incoming signal  $I$  is directly available.

Returning to FIG. 12, it should be understood that the Hilbert transform circuit 180  
introduces some measure of delay in the signal path between the input to the decision device 176  
in the input to the multiplier 182 for combination with an error term  $E_i$ . An arbitrary delay  
15 introduced in any one leg of the signal paths would thus contribute a delay term (an additional  
error term) to the output phase error term  $P_i$  which would have the effect of either over or under  
compensating any phase lead or phase lag exhibited by the incoming signal. Accordingly, an  
additional delay stage 190 is introduced between the output of the summing junction 178 and the  
multiplier 182 in order to match the delay introduced by the Hilbert transform circuit 180. Since  
20 the phase detection and correction circuit of FIG. 12 is immanently suitable for implementation  
in integrated circuit technology, the delays caused by the Hilbert transform circuit 180 can be  
calculated to a reasonable degree of accuracy. Once delay has been characterized, a suitable  
matching delay can be devised by constructing the delay stage 190 with similar integrated circuit  
components having similar response characteristics and parasitic resistances and capacitances to  
25 the Hilbert transform circuit 180.

It should be understood that in carrier recovery systems based on the pilot, both QAM and  
VSB constellations are able to be accurately decoded so long as the phase of the pilot accurately  
represents the average phase of the signals. However, as is well understood by those having skill  
in the art, typical communication channels exhibit a non-linear phase response causing the pilot  
30 to often be attenuated. The channel phase response at the pilot location is quite often different  
from the channel phase response elsewhere along the spectrum, thus causing a constellation to  
be effectively rotated when evaluated in connection with pilot phase. Since a systems' equalizer  
is expecting true baseband from the pilot, the system response might be accurately characterized  
with respect to pilot frequency but not necessarily accurately with respect to pilot phase, i.e., the  
35 system exhibits pre-equalizer rotation. Since the Equalizer is expecting to receive a signal that  
might be characterized as  $A(t)e^{j\omega t + \phi}$ , where the first portion of the exponential term represents  
frequency and the second portion of the exponential term represents phase.

1 In order to minimize pre-equalizer rotation, the dual mode QAM/VSB receiver according  
to the invention incorporates a 1-tap LMS derotater in OQAM mode in order to perform a pre-  
equalizer phase correction. Turning now to FIG. 13 and with reference to the exemplary  
embodiment of a dual mode QAM/VSB receiver of FIG. 9, the 1-tap LMS derotater is suitably  
5 disposed in the signal path before the equalizer 24 (also identified with the same reference  
numeral in the exemplary embodiment of FIG. 9). Complex signals I and Q are evaluated in a  
decision device 200 that is implemented in the exemplary embodiment of FIG. 13 as a slicer.  
Input complex signals I and Q are negatively combined with quantized QPSK symbol values in  
a summing junction 202 in order to define a complex error term  $E$ . Complex error  $E$  is processed  
10 by a least means squares (LMS) function block 204 to develop a rotational alpha  $\alpha$  having the  
conventional representation  $\alpha_{n+1} = \alpha_n - \mu \cdot X^* \cdot E$ , where  $\mu$  represents the step change.

$\alpha$  is applied to a complex multiplier 206 where it is used to provide any needed pre-  
equalizer rotation correction before the complex signals I and Q are directed to the equalizer  
circuit 24.

15 As discussed above in connection with FIG. 9, the dual mode QAM/VSB receiver  
according to the invention incorporates a decision feedback equalizer (24 of FIGs. 1 and 9) which  
is suitably constructed of a feedforward filter section (or FFE) and a decision feedback filter  
section (or DFE) as is illustrated in the simplified, semi-schematic exemplary embodiment of FIG.  
14. In particular, an input signal, represented as  $x_{\text{FFE\_in}}$  is directed to a feedforward filter  
20 element 200. After filtering, the signal is summed with the negative of the output of a decision  
feedback filter element 202 in a complex summing junction 204. Summed signals are directed  
to the input of a decision device 206, such as a multi-level slicer, which provides a signal  
decision, denoted  $x_{\text{dec}}$ , at one output and an error term, denoted "error", representing a vector  
difference between a valid, quantized constellation point and an actual received value. Decisions  
25 developed by the slicer 206 are further directed to the input of a decision feedback filter element  
(DFE) as a parallel signal denoted a DFE word, and identified as  $dfe\_w$ . Thus, as is well  
understood by those having skill in the art, the received signal  $x_{\text{ffe\_in}}$  is only used by the  
feedforward filter element 200, while an estimated decision signal  $x_{\text{dec}}$  is used by the decision  
feedback filter element 202. At the summing junction 204, an FFF filter version of the tail  
30 portion of the channel impulse response is canceled by the DFF weighted estimated signals. Any  
noise enhancement introduced by a DFE is only caused by equalization of the remaining smaller  
portion of the channel impulse response. As is also well understood, a feedforward filter (FFF)  
compensates for channel distortion with linear equalization and can be implemented at multiples  
of the baud rate. Decision feedback filters (DFF) cancel the tail portion of the channel impulse  
35 response using recovered data symbols. As such, a DFF can be implemented only at the baud  
rate.

No matter how implemented, the decision feedback filter element 202 is a highly complex  
system which performs a significant number of arithmetic calculations, at extremely high

1      clocking speeds. The number of calculations performed necessarily depends upon both the length  
 of the filter, i.e., the number of coefficients (or taps) that contribute to the final output signal, as  
 well as the width of the filter, represented by the filter's wordlength or the number of bits  
 required for representation of the symbols at the input of the DFE. Reducing the wordlength of  
 5      the decision feedback filter 202 significantly reduces the complexity of the decision feedback  
 filter block.

FIG. 15 is a simplified block level diagram illustrating an exemplary 8-tap decision  
 feedback filter, suitably implemented as a sequential string of delay stages, with the output of  
 each delay stage, as well as symbols at the DFF input, each being multiplied by a corresponding  
 10      coefficient, denoted  $d(0)...d(7)$ . Each of the coefficient multiplied signals are summed together  
 at summing junctions in order to define a filter output  $y(n)$ . It should be understood that  
 $d(0)...d(7)$  denotes 8 multiplication operations, each of which require significant investments in  
 processing hardware, and each of which are performed in parallel fashion with an index equal  
 to the decision feedback filter word length  $dfe\_w$ . The hardware complexity of these  
 15      multiplication operations are linearly reduced when the word length  $dfe\_w$  is reduced.

QAM modulated signals include an in-phase component and a quadrature-phase  
 component, denoted I and Q respectively, which requires the use of a complex decision feedback  
 equalizer such as depicted in semi-schematic block diagram form in FIG. 16. Briefly, the  
 exemplary complex decision feedback equalizer of FIG. 16 includes real and imaginary filters  
 20      for each of the in-phase and quadrature-phase input components. For example, an in-phase signal  
 $I_{in}$  is processed by a real filter 208 whose output is summed with the output of an imaginary filter  
 212 which receives a quadrature-phase input. Likewise, the quadrature-phase input is processed  
 by a real filter 214 whose output is summed with the output of an imaginary filter 210 which, in  
 turn receives an in-phase signal  $I_{in}$  as an input. Thus, it should be understood that the exemplary  
 25      complex decision feedback equalizer of FIG. 16 is nothing more than a graphical, block diagram  
 representation of the mathematical function defining a complex filter.

In the case where the exemplary complex decision feedback equalizer of FIG. 16 is  
 operating on a 256 QAM signal, 8-bits are required to adequately define the representation of  
 each symbol at the input to the exemplary complex dfe. This is because 256 QAM symbols  
 30      requires  $\text{LOG}_2(256) = 8$ -bits for symbol representation. The 8-bit representation of each symbol  
 can be divided into two subsets, with 4-bits chosen to represent real symbols (denoted as in-phase  
 or I symbols) and 4-bits chosen to represent imaginary symbols (denoted as quadrature-phase or  
 Q symbols). When represented in this manner, a 256 QAM constellation might appear as  
 depicted in the graphical representation of FIG. 17, and suitably includes the  $2^4 = 16 \times 16 = 256$   
 35      complex symbols, symmetrically arranged about the I and Q axis.

In order to maintain the symmetry about the zeros of the I and Q axis, as well as for ease  
 of numerical processing, the binary two's complement numbering system is used for  
 implementing the signal processing functions in the exemplary dual mode QAM/VSB receiver.

Utilizing two's complement as the numbering system, results in a  $-1/2$  bit offset in representation of each of the QAM symbols. As can be determined from the exemplary 256 QAM constellation represented in FIG. 17, quantized symbol points (desired symbols) range from  $-15/16$  to  $15/16$  on both the I and Q axes with a  $1/8$  offset, or separation, between symbol points. Thus, an input signal  $x(n)$  would take on values of  $\{-15/16, -13/16, -11/16, -9/16, -7/16, -5/16, -3/16, -1/16, 1/16, 3/16, 5/16, 7/16, 9/16, 11/16, 13/16, \text{ and } 15/16\}$ .

However, a 4-bit representation of each of the 256 QAM symbol points in the two's complement numbering system can be expressed as  $\{100_b, 1001_b, 1010_b, 1011_b, 1100_b, 1101_b, 1110_b, 1111_b, 0000_b, 0001_b, 0010_b, 0011_b, 0100_b, 0101_b, 0110_b, 0111_b\}$  which, when expressed in common numerical form represents an input signal, denoted by  $z(n)$ , which takes on the discrete values  $\{-16/16, -14/16, -12/16, -10/16, -8/16, -6/16, -4/16, -2/16, 0, 2/16, 4/16, 6/16, 8/16, 10/16, 12/16 \text{ and } 14/16\}$ . Thus, it will be understood that the effective input signal  $z(n)$ , when processed, would give symbol quantization results that are incorrect by a fixed offset, equal to  $-1/16$ , and which is denoted herein by  $a$ . Since  $-1/16$  may be represented by the binary value 00001 in two's complement, the  $-1/16$  fixed offset may be corrected by adding  $a=00001$  to  $z(n)$  as a correction factor.

While effective to some degree, adding a correction factor in this manner raises the number of bits required to represent each I and Q symbol from 4-bits to 5-bits for each discrete symbol point. Thus, an input signal  $x(n)$  that accurately represents discrete symbol points would be represented by  $\{10001, 10011, 10101, 10111, \dots, 01001, 01011, 01101, \text{ and } 01111\}$  which correctly represents the desired discrete symbol values from  $-15/16$  to  $15/16$ . However, increasing the wordlength required to accurately represent a symbol from 4-bits to 5-bits linearly increases the complexity of the multipliers used to implement the decision feedback filter portion of the system's DFE.

In accordance with the invention, a decision feedback equalizer (DFE) constructed in accordance with the simplified, block diagram of FIG. 18, includes a decision feedback filter 220 that accommodates a two's complement representation of discrete symbol points in a manner that minimally effects the increase in hardware complexity caused by the two's complement numbering system. In the exemplary embodiment of the DFE of FIG. 18, an input signal  $x\_ffe\_in$  is received by a feedforward filter 222, having a coefficient set represented by  $f(n)$ . The feedforward filter's output is directed to a decision device 224, such as a slicer, configured to output a tentative decision, represented by  $x\_dec$  and an error term. Tentative decisions are directed to the input of a decision feedback filter 220 in the form of an input signal, denoted  $x(n)$ , which may be alternatively described as a DFE word represented as  $dfe\_w$ . However, and in accordance with the invention, the DFE word is a 4-bit representation and, thus, does not include the fifth bit fixed offset term denoted by  $a$ . Thus, the DFE word is represented in the exemplary embodiment of FIG. 18 as  $dfe\_w-a$ .



1           Returning momentarily to the exemplary decision feedback filter of FIG. 15, it will be realized that such a filter, with input  $x(n)$ , output  $y(n)$ , and coefficients  $d(n)$  can be characterized by the convolutional equation  $y(n) = \sum_k d(k)x(n-k)$ . However, if the input signal to the exemplary filter of FIG. 15 is viewed as including an input stimulus portion and a fixed offset portion, the  
 5           input signal could be expressed as  $x(n) = z(n) + a$ . Given this particular mathematical relationship, and substituting terms in the filter response characteristic, the filter output might be represented as  $y(n) = \sum_k d(k)z(n-k) + \sum_k d(k)a$ , where  $a$  represents the fixed offset term and  $z(n)$  represents the input stimulus.

          From the above, it will be evident that the filter's output might be expressed as the sum  
 10          of two independent terms, a first term in which the input stimulus  $z$  is convolved with the coefficient set  $d$  and a second term in which the coefficient set  $d$  is convolved with the fixed offset term  $a$ . When separated, the first portion of the filter's response characteristic retains the original representational word length (4-bits according to the foregoing exemplary description) which is directed to the input of the decision feedback filter 220 of the exemplary embodiment  
 15          of the DFE of FIG. 18. The characteristic filter output  $y(n)$  is developed in a summing node 226 which sums the output of the decision feedback filter 220 with the output of an offset generation circuit 228 which provides an offset correction signal equal to the convolution of the decision feedback filter coefficients  $d$  with the fixed offset term  $a$ . Thus, an offset equal to  $\sum_k d(k)a$  is added to the output of the decision feedback filter 220 at the summing junction 226 down-stream  
 20          from the output of the decision feedback filter.

          The offset cancellation circuit 228 might be constructed as a simple register which receives adaptively defined coefficients  $d(n)$  from the decision feedback filter 220. Coefficient values are multiplied by the fixed offset  $a$  and summed for all  $k$  to define the offset term added to the output of the decision feedback filter. Accordingly, intensive numerical processing,  
 25          performed by the decision feedback filter 220, is performed on a DFE wordlength of only 4-bits. Processing required to generate the offset term is minimal and requires a significantly lower investment in computational hardware than if the offset term were incorporated in the DFE word as a fifth bit. Computational complexity is significantly reduced as a consequence.

          The decision feedback filter output  $y(n)$ , which includes the offset term, is negatively  
 30          summed with the output of the feedforward filter 222 at a summing circuit 230. The sum of the negative of the decision feedback filter output and the feedforward filter output is provided as an input to the slicer 224. It bears mentioning that the error term developed by the slicer 224 is provided as a control input to both the decision feedback filter 220 and the feedforward filter 222 for adaptively modifying the content of the coefficient registers such that the decision feedback  
 35          filter and feedforward filter converge. Needless to say, the adaptively reconfigured coefficients  $d(n)$  of the decision feedback filter 220 are provided to the offset cancellation circuit 228 to accurately correlate the offset term to the output of the decision feedback filter. The extent of the reduction in computational complexity of the filters in a DFE constructed in accordance with

1 the invention might be better understood when it is recognized that the exemplary dual mode  
QAM/VSB receiver includes a 496-tap decision directed equalizer having 64 feedforward taps  
and 432 feedback taps. A 20% reduction in the decision feedback filter circuitry (reducing the  
DFE wordlength from 5-bits to 4-bits) more than compensates for the minimal additional  
5 hardware required by the offset cancellation circuit 228.

The foregoing discussion was concerned with reducing the computational complexity of  
DFE elements that might otherwise have obtained as a result of carrying forward a fixed offset  
value of a two's complement representation of a 256 QAM constellation. In the case of VSB  
modulated signals, the same type of symbol representational offset occurs with regard to a VSB  
10 constellation, as well as a DC offset term introduced as an artifact of the above-described pilot.  
The ATSC standard for VSB transmission requires utilization of a pilot tone as a carrier  
reference. When a received spectrum is mixed down to baseband, the pilot tone reduces to a DC  
component at baseband and which must consequently be subtracted from an equalizer signal prior  
to its introduction to the slicer and subsequently added back to the decision signal defined at the  
15 slicer output.

FIG. 19 is a simplified block level diagram of a DFE similar to the exemplary embodiment  
of FIG. 18, but further including a pilot tone generation circuit 232 which functions to develop  
a DC component equal to the pilot's DC component baseband. The DC component developed  
by the pilot tone generation circuit 232 is negatively summed with the filtered DFE input in a  
20 summing circuit 234 prior to the signals being directed to the slicer 224. The DC component  
developed by the pilot tone generation circuit 232 is further added to the tentative decision  $x_{dec}$   
developed by the slicer, in summing circuit 236, prior to the decisions being provided to the input  
of the decision feedback filter 220 and also prior to its being output from the DFE for decoding  
and error correction. The DC component, thus added to the decision value has the effect of  
25 increasing the DFE wordlength at the input to the decision feedback filter 220. In the case of 8  
VSB the discrete symbol values might be represented as  $\{-7/8, -5/8, -3/8, -1/8, 1/8, 3/8, 5/8, \text{ and } 7/8\}$   
with the value of the pilot tone generally recognized as  $5/32$ . In ordinary binary terms, the  
DFE wordlength that would be necessary to represent 8 VSB symbols is 3-bits. However,  
utilizing the two's complement numbering system results in a  $-1/8$  offset, in a manner similar to  
30 the QAM case described above, which requires an additional bit for its representation, resulting  
in 4-bits being required to accurately represent each of the 8 VSB constellation points. When the  
pilot tone value is factored into the foregoing, it should be understood that the pilot tone further  
increases the DFE wordlength by adding  $5/32$ , or  $000101_2$ , in two's complement representation,  
to each symbol value, resulting in a 2-bit increase to the wordlength (thus increasing the  
35 wordlength from 4-bits to 6-bits). Thus, the DC pilot tone component of  $5/32$ , in combination  
with the fixed  $-1/8$  symbol offset, necessitates an approximately 50% increase in the  
computational complexity of a decision feedback filter of a DFE operating on 8 VSB modulated  
signals.

1 Turning now to FIG. 20, an additional exemplary embodiment of a decision feedback equalizer, configured for VSB modulated signals, and constructed to reduce DFE wordlength from the nominal 3-bit case back to an original 3-bit representation, is illustrated in simplified, semi-schematic block diagram form. In particular, the pilot tone generation circuit 232 develops  
5 a DC component equal to the pilot tone DC component at baseband, and provides the component value to a summing circuit 240, where it is subtracted from the filtered DFE signal prior to its introduction of the slicer 224. However, and in accordance with the invention, the pilot tone generation circuit 232 is decoupled from the decision output of the decision slicer 224 and instead provides the DC component corresponding to the pilot tone to an offset correction circuit  
10 242 which functions to compensate the output of the decision feedback filter 220 with an offset term  $a$  equal to the value of the pilot tone minus the  $1/8$  offset introduced by the two's complement numbering system.

In general terms, the same mathematical analysis may be performed on the DFE exemplified in FIG. 20 as was performed on the DFE exemplified in FIG. 18. Specifically, the  
15 tentative decision  $x_{dec}$  is provided to the decision feedback filter 220 as a 3-bit DFE word,  $dfe\_w-a$ , that does not include the 2-bits representing the  $-1/8$  computational offset and the  $5/32$  pilot tone value. The pilot tone and computational offset values are convolved with the filter's coefficient values in order to define an offset term which is summed with the filter output in a summing circuit 244 to define a decision feedback filter output  $y(n)$ . The DFF output  $y(n)$  is  
20 subtracted from the output of the feedforward filter 222 in the summing circuit 230 prior to its introduction to the slicer 224.

Not only does the offset correction circuit 242 function to significantly reduce the complexity of the decision feedback filter 220 in the VSB case, but it also allows the pilots on generation circuit 232 to be decoupled from the slicer's output. In the conventional DFE  
25 embodiment of FIG. 19, the pilot tone value is added back to the slicer output prior to the tentative decision's being provided to the decision feedback filter because the pilot tone value is subtracted from the slicer's input signal, after the decision feedback filter output has been combined with the feedforward filtered input signal. The DC component removed from the signal after the decision feedback filter 220 must be replaced in order that the filter remain  
30 converged.

In the exemplary embodiment of FIG. 20, pilot tone DC compensation, as well as computational offset computation, occurs in a loop disposed inside the feedback loop of the decision feedback filter, as well as occurring prior to the slicer 224. Thus, pilot tone DC compensation occurs twice in the signal path between the decision feedback filter output and the  
35 input to the slicer; a first compensation associated with the offset correction circuit 242, where a compensation term related to the pilot term is added to the output of the decision feedback filter, and a second compensation occurring just prior to the input of the slicer where the pilot tone DC component is removed from the input signal. Completely removing the pilot tone DC

1 component from the signal within the DFE is further advantageous in that there is not DC offset present in signals provided to the decoder and forward error correction (FEC) circuitry following the DFE. Additional savings in the complexity of FEC and decoder circuitry can be realized by obviating the requirement that a signal from the DFE be processed with DC offset components.

5 Trellis coded modulation is employed in modern digital communication systems to improve a system's bit error rate in high noise situations. Trellis coded modulation (TCM) achieves a performance gain by increasing the size of a constellation within the modulation scheme, thereby increasing the "distance" between possible transmitted sequences. A particular example of a TCM communication system might include the U.S. digital terrestrial broadcasting standard, which employs a trellis coded 8 VSB modulation scheme. The particular code used has  
10 an asymptotic coding gain of 3.31db over uncoded 4 VSB.

FIG. 21 is a simplified, semi-schematic block diagram of an exemplary encoder which might be provided in a typical terrestrial broadcast transmitter, and which might be represented in simplified form as a convolutional encoder 300 in combination with a signal mapper 302. A  
15 2-bit input signal,  $Y_1$  and  $Y_2$ , are input to the convolutional encoder 300 with the least significant bit,  $Y_1$ , also directed, in parallel fashion, through a convolutional encoder, implemented as a linear feedback shift register, in order to generate a redundancy bit which is a necessary condition for the provision of coding gain of the code.

As described above, the convolutional encoder 300 includes a linear feedback shift  
20 register, constructed of two delay elements 304 and 306 (conventionally denoted by  $Z^{-1}$ ) separated by a summing circuit 307, which function to combine the least significant bit  $Y_1$  of the input word with the output of the delay elements 304 and 306. The time sequence formed by the LSB bit stream is convolved with the coefficients of the linear feedback shift register in order to produce the time sequence of the redundancy bit. Thus, the convolutional encoder might be  
25 viewed as a state machine.

The signal mapper 302 maps the resulting 3 bits,  $Z_2$ ,  $Z_1$ , and  $Z_0$  into a particular constellation level. Since there are 3-bits coming into the symbol mapper 302, a maximum of 8 levels might be represented by combinations of the 3-bits. As will be understood from the block diagram of FIG. 21, the 8 possible levels might be represented as -7, -5, -3, -1, 1, 3, 5 and  
30 7.

However, since coding increases signal modulation from 4 levels to 8 levels, decision directed loops, such as decision directed adaptive equalization, decision directed carrier and/or timing recovery loops, and the like, are forced to function with respect to an increased constellation size of 8 levels.

35 Turning now to FIG. 22, an exemplary decision directed carrier and timing recovery loop is shown in simplified, semi-schematic block diagram form, and includes a symbol-by-symbol slicer 310 as a decision device, operating in combination with a DFE 312 to generate tentative decisions suitable for use by a carrier loop 314 and timing loop 316. However, at signal-to-noise

1 ratios (SNR) near system threshold, the loops will fail due to the combination of higher noise and  
larger constellation size. As a result, the system will not be able to achieve adequate lock, and  
the expected coding gain from TCM would not be realized. In particular, a symbol-by-symbol  
slicer does not employ sequence estimation in generating symbolic decisions. Rather, it operates  
5 only upon the "current" symbol, ignoring any past decisions.

On the other hand, were the DFE input to be taken from a best survivor path in a trellis  
decoder's trace back memory, the system would be able to exploit the correlations between a  
"current" symbol and past decisions, by maximum likelihood sequence estimation, for example.  
The DFE input would thus exhibit a lower error rate and, with a higher percentage of correct  
10 decisions, the DFE's ability to operate in low SNR environments is enhanced.

Turning now to FIG. 23, there is shown in simplified, semi-schematic block diagram form,  
a generalized decision feedback equalizer circuit that includes a TCM demodulation circuit, also  
termed a Viterbi decoder, which provides the input to a decision feedback equalizer 322. The  
system includes a carrier loop 324 that drives a derotater 326 disposed between the Viterbi 320  
15 and a feedforward equalizer 328.

In addition to the carrier loop 324, the system also includes a symbol timing loop 330,  
coupled to provide a symbol timing reference to a variable interpolating filter 332. Although the  
symbol timing loop 330 is depicted in the exemplary embodiment of FIG. 23, the symbol timing  
loop 330 need not be decision directed, in the context of the present invention, but might  
20 alternatively be configured to operate upon an enhanced pilot signal in a manner described in  
connection with FIGs. 4 and 9.

In accordance with the invention, the input and output of the Viterbi 320 is directed to a  
summing junction 334 which combines an input signal and a tentative decision from the Viterbi  
in order to generate an error term. The error term, in turn, is used to drive the coefficient tap  
25 update of the FFE 328, as well as the coefficient tap update of the DFE 322. Providing a lower  
probability of error in the tap update signal significantly improves the performance and reliability  
of the FFE 328.

As will be described in greater detail below, TCM decoders exhibit a tradeoff between  
system delay and the reliability of symbolic decisions. In general, making use of decisions farther  
30 back in the history of a TCM demodulator tends to increase the reliability of the decision, with  
most reliable decision being the final decision. However, each stage in the process involves a  
certain amount of delay and it is sometimes desirable to choose decisions from some intermediate  
point of the traceback history. The earlier the chosen decision, the less the consequent delay.  
Accordingly, variable delay circuits 336a, 336b and 336c are provided between the input of the  
35 Viterbi 320 and the summing junction 334, the carrier loop 324 and the timing loop 330. The  
variable delay circuits 336a, b and c function to match the delay of the chosen symbol output  
from the Viterbi such that the summing junction 334, carrier loop 324 and timing loop 330  
operate on signals having the same time stamp.

1           Turning now to FIG. 24, a TCM decoder, or Viterbi decoder, is depicted in semi-  
schematic, block diagram form at 320. A Viterbi suitably includes a decision device 340 coupled  
to receive an input signal from an FFE 328 that has been summed with the output of a DFE 322  
in a summing junction 342. A Viterbi decoder processes information signals iteratively, tracing  
5           through a trellis diagram corresponding to the one used by the encoder, in an attempt to emulate  
the encoder's behavior. At any particular time frame, the decoder is not instantaneously aware  
of which node (or state) the encoder has reached. Thus, it does not try to decode the node at that  
particular time frame. Instead, given the received sequence of signal samples, the decoder  
calculates the most likely path to every node and determines the distance between each of such  
10          paths and the received sequence in order to determine a quantity called a path metric.

          Further, the Viterbi 320, in accordance with the invention, makes an assumption that the  
surviving paths at the Nth time frame pass through a common first branch and outputs a decision  
for time frame 0 on the basis of that assumption. If this decision is incorrect, the Viterbi 320 will  
necessarily output a few additional incorrect decisions based on the initial perturbation, but will  
15          soon recover due to the nature of the particular relationship between the code and the  
characteristics of the transmission channel. It should be noted, further, that this potential error  
introduction source is relatively trivial in actual practice, since the assumption made by the  
Viterbi that all surviving paths at time frame n pass through a common first branch at time frame  
0, as a correct one to a very high statistical probability.

20          In FIG. 24, the exemplary trellis decoder (or Viterbi) 320 further includes a path metrics  
module 344 and a path memory module 346 in addition to the decision device 340. A path  
metric, as the term is used herein, is well known and refers to a plurality of elemental paths  
between neighboring trellis nodes, which form, by extension, a path. The Viterbi selects the best  
path for each incoming signal and updates a path memory stored in the path memory module 346  
25          and the path metrics stored in the path metrics module 344. It will, thus, be understood that the  
path (or trace) memory module 346 includes a historical record of a particular number of past  
decisions, with the number of past decisions represented by a depth parameter N.

          Any one of a number of historical decisions may be taken from the path memory 346 and  
provided both to the DFE 322 and an error term generating summing junction 334 by selecting  
30          the appropriate historical signal through a multiplex circuit 348.

          Turning now to FIG. 25, the TCM demodulator (or Viterbi) 320 might be considered as  
including 4 traceback registers, with each traceback register specific to a particular one of the 4  
states making up the 8 VSB signal. A MUX 348 selects one of the 4 traceback registers,  
corresponding to the one containing the most likely symbol, in accordance with a select signal  
35          defined by the path metrics module (344 of FIG. 24). The particular symbolic decision chosen  
by the MUX 348, is output from the TCM demodulator and provided to the DFE 322 where it  
is combined with a set of N non-causal coefficients, where N represents the length N of each of  
the traceback registers. Further, the output symbolic decision from the TCM demodulator 320

1 is processed by a set of  $M + 1$  causal coefficients in the DFE 322, where  $M$  represents the difference between the total number of coefficient taps and the length of the traceback register (the number of non-causal taps).

5 Further, the output of the TCM demodulator 320 is provided to a summing junction 334 where its value is combined with the TCM demodulator input in order to define an error term based upon the difference between an input signal sample and an output symbolic decision. This error term is then provided to both the DFE 322 and an FFE 328 where it is used to update the tap coefficients.

10 As was mentioned earlier, symbolic decisions may be taken from each of the traceback memories at any one of the intermediate steps in the process. Depending upon the sequential position of the actual symbolic decision tap, a certain delay can be determined and that amount of delay is accommodated in a delay circuit 350 disposed between the input of the TCM demodulator 320 and the summing junction 334 in order that the time stamp of the input signal and the time stamp of the symbolic decision to be summed are equal. This delay is variable and  
15 programmable in that circuit simulations may be run in order to determine the delay/performance tradeoff characteristics. Either performance or delay (or a mixture of both) might be set as a decision metric and the system optimized for either maximum performance, minimum delay, or an adequate value of both. It is indicated in the exemplary embodiment of FIG. 23, the symbolic decisions, and consequent delay, need not necessarily be the same for defining the error term,  
20 providing an input to the carrier loop or the timing loop. Indeed, because of the different bandwidth constraints and acquisition characteristics of a carrier loop and a timing loop, it should be understood that the carrier loop needs to acquire at a much faster rate than the timing loop, allowing the timing loop to use a more "downstream" survivor path in the trellis decoder's path memory module and not be too concerned with its attendant delay.

25 In the case of a carrier loop, using decisions farther back in the history of the TCM decoder would tend to increase the reliability of decisions. However, increasing delay in the carrier loop correspondingly reduces the loop's tracking ability. Thus, the variable delay feature of the invention enhances overall system performance of a multi-loop decision directed system, as well as providing improved equalization characteristics.

30 The foregoing discussion discloses and describes merely exemplary methods and embodiments of a dual mode QAM/VSB receiver in accordance with the present invention. As will be understood by those familiar with the art, the various features and functions of the invention may be embodied in a variety of other specific forms without departing from the spirit or essential characteristics thereof. Accordingly, the disclosure of the present invention is  
35 intended to be illustrative of, but not limiting to, the scope of the invention, which is set forth in the following claims.

## 1 CLAIMS

1. A method for operating a receiver having a particular sampling frequency related to a symbol rate to recover carrier and timing information from a received spectrum including a pilot signal, comprising:
- 5 centering the received spectrum at a known position relative to baseband;  
tracking the pilot signal with a phase-lock-loop;  
evaluating the frequency of the pilot signal with respect to the sampling frequency;  
and  
10 adjusting the centering of the received spectrum until the evaluated frequency of the pilot is in integral relationship with the sampling frequency.
2. The method according to claim 1, further comprising:  
filtering the received spectrum in a low pass filter having a cut-off frequency related to the sampling frequency;  
15 processing the filtered signal in a high pass filter having a cut-off frequency related to the sampling frequency; and  
wherein the low pass and high pass filters define an equivalent bandpass filter, the equivalent bandpass filter defining upper and lower sideband regions each centered at an expected position of the pilot signal.  
20
3. The method according to claim 2, wherein the received spectrum exhibits a raised cosine response characteristic, the upper and lower sideband regions of the equivalent filter including transition regions of the spectra defined by the high pass and low pass filters.  
25
4. The method according to claim 3, wherein the receiver's sampling frequency is determined such that the pilot frequency is equal to about one fourth the sampling frequency.
5. The method according to claim 4, wherein the high pass filter is a Nyquist prefilter having a lower cut-off frequency at about one fourth the sampling frequency, the high pass filter centering the spectrum at a frequency about one half the sampling frequency.  
30
6. The method according to claim 5, wherein the low pass filter is a square root Nyquist filter having an upper cutoff frequency at about one fourth the sampling frequency, the square root Nyquist filter centering the spectrum at about baseband.  
35
7. The method according to claim 6, the desired position of the pilot signal being substantially centered in each transition region, thereby causing the desired position of the pilot



1 signal to be centered in each of the upper and lower sideband regions of the equivalent filter at a frequency substantially equal to one fourth the sampling frequency, thereby augmenting a signal occurring at one fourth the sampling frequency.

5 8. The method according to claim 7, further comprising:  
receiving a sideband region from the equivalent filter in a tracking loop;  
sweeping the sideband region to identify an augmented frequency component;  
comparing the augmented frequency component to the expected frequency of the  
pilot signal; and

10 shifting the sampling frequency in a direction and an amount such that the augmented frequency component coincides with the expected frequency of the pilot signal.

9. The method according to claim 8, further comprising the step of using the shifted sampling frequency to define a symbol timing reference signal.

15 10. A digital communication system, comprising:  
a front end receiving an input spectrum at an intermediate frequency, the input spectrum including an inserted predetermined frequency component;  
first and second nested tracking loops, the first loop acquiring carrier frequency  
20 lock in operative response to the predetermined frequency component of the received spectrum, the second loop providing a signal adapted to position the spectrum at a predetermined location relative to baseband in operative response to said predetermined frequency component; and  
a third tracking loop coupled to define a symbol timing parameter in operative response to said same predetermined frequency component.

25 11. The digital communication system according to claim 10, further comprising an equivalent filter operating on the received spectrum in order to define a pair of symmetric signals, each of the symmetric signals centered at the characteristic frequency of the predetermined frequency component when the received spectrum is at baseband.

30 12. The digital communication system according to claim 11, wherein symbol timing is performed at a sampling frequency, the system further comprising:

a first high pass filter having a lower cut-off frequency related to the sampling frequency;

35 a second low pass filter having an upper cut-off frequency related to the sampling frequency; and

wherein the first and second filters define an equivalent bandpass filter having symmetric passband regions centered about a frequency related to the sampling frequency.

1           13. The digital communication system according to claim 12, wherein the received spectrum exhibits a raised cosine response characteristic, the passband regions including the transition regions of the high and low pass filtered spectra.

5           14. The digital communication system according to claim 13, wherein the sampling frequency is chosen such that the predetermined frequency component is disposed at a frequency one fourth the sampling frequency.

10           15. The digital communication system according to claim 14, wherein the high pass filter has a lower cut-off of about one fourth the sampling frequency and a passband center of about one half the sampling frequency.

15           16. The digital communication system according to claim 15, wherein the low pass filter has an upper cut-off of about one fourth the sampling frequency, the equivalent filter passbands thereby centered at a frequency about one fourth the sampling frequency.

20           17. The digital communication system according to claim 16, wherein the inserted predetermined frequency component is a pilot signal disposed at a location along the spectrum normally reserved for a suppressed carrier when the spectrum is a conventional terrestrial broadcast spectrum, the pilot signal centered in the equivalent filter's passband regions when the sampling frequency is one fourth the frequency of the pilot signal.

25           18. The digital communication system according to claim 17, further comprising:  
a phase/frequency detector coupled to receive an equivalent filter passband signal;  
means for determining whether the pilot is centered in the passband region; and  
an oscillator circuit developing a timing reference signal having a frequency related to the sampling frequency, the oscillator circuit increasing or decreasing the timing reference signal frequency in operative response to the position of the pilot signal with respect to a passband region center.

30           19. An integrated circuit receiver including a decision directed carrier phase recovery circuit for complex signals representing symbols characterized by in-phase and quadrature-phase portions separated in time by an offset, the carrier phase recovery circuit comprising:

35           a sampling circuit configured to sample each of the in-phase and quadrature-phase portions of the complex signal at an in-phase sampling time and at a quadrature-phase sampling time separated by an offset;

a separation circuit, connected to separate the sampled, in-phase, signal into an in-phase sample time data stream and an in-phase time offset data stream;

- 1                   a decision circuit, connected to receive the in-phase sample time data stream and  
generate a tentative symbolic decisions from in-phase sampled data;  
                  a summing circuit coupled to combine the tentative symbolic decisions with signals  
from the in-phase sample time data stream to generate an in-phase symbolic error term;  
5                   a multiplier circuit connected to combine the in-phase symbolic error term with a  
time offset signal representing the quadrature-phase portion of the complex signal.
20.   The carrier phase recovery circuit according to claim 19, further comprising:  
          a phase error term representing the in-phase portion, generated by the multiplier;  
10           a loop filter;  
          a reference synthesizer circuit; and  
          a phase correction circuit, the reference synthesizer providing phase correction  
signals to the phase correction circuit in operative response to the phase error term.
- 15           21.   The carrier phase recovery circuit according to claim 19, further comprising:  
          a second separation circuit, connected to separate the sampled, quadrature-phase,  
signal into a quadrature-phase sample time data stream and a quadrature-phase time offset data  
stream;  
          a second decision circuit, connected to receive the quadrature-phase sample time  
20           data stream and generate a tentative symbolic decisions from quadrature-phase sampled data;  
          a second summing circuit coupled to combine the tentative symbolic decisions with  
signals from the quadrature-phase sample time data stream to generate a quadrature-phase  
symbolic error term;  
          a second multiplier circuit connected to combine the quadrature-phase symbolic  
25           error term with the a time offset signal representing the in-phase portion of the complex signal.
22.   The carrier phase recovery circuit according to claim 21, wherein the second  
multiplier circuit combines the quadrature-phase symbolic error term with the in-phase time  
offset signal to develop a quadrature-phase phase error term.
- 30           23.   The carrier phase recovery circuit according to claim 22, further comprising a  
multiplexer connected to each multiplier circuit, the multiplexer providing a signal stream of  
alternating in-phase and quadrature-phase phase error terms to the loop filter.
- 35           24.   The carrier phase recovery circuit according to claim 20, wherein the time offset  
signal representing the quadrature-phase portion of the complex signal is the sign of a quadrature-  
phase time offset data stream.

1           25    The carrier phase recovery circuit according to claim 20, wherein the time offset  
signal representing the quadrature-phase portion of the complex signal is a quadrature-phase time  
offset data stream.

5           26.   The carrier phase recovery circuit according to claim 20, wherein the time offset  
signal representing the quadrature-phase portion of the complex signal is the Hilbert transform  
of the in-phase sample time data stream.

10           27.   The carrier phase recovery circuit according to claim 20, further comprising:  
a Hilbert transform circuit connected to receive the in-phase sample time data  
stream and output its Hilbert transform, wherein the time offset signal representing the  
quadrature-phase portion of the complex signal is the Hilbert transform of the in-phase sample  
time data stream; and

15                wherein the multiplier combines the symbolic in-phase error term with the Hilbert  
transform of the in-phase sample time data stream.

28.   The carrier phase recovery circuit according to claim 27, further comprising:  
a DFE coupled, in parallel fashion, with the decision device, the DFE providing  
correction signals for removing an ISI component from tentative symbolic decisions; and  
20           a combining circuit coupled to combine DFE correction signals with in-phase  
sample time data.

29    The carrier phase recovery circuit according to claim 27, further comprising a delay  
matching circuit disposed between the summing circuit and the multiplier, the delay matching  
25    circuit providing a delay to the symbolic in-phase error term equal to a delay imposed by the  
Hilbert transform circuit.

30           30.   In an integrated circuit receiver for coherently demodulating complex signals  
representing symbols, characterized by first-phase and second-phase portions, separated in time  
by an offset, a method for decision directed carrier phase recovery comprising:

30                sampling each of the first-phase and second-phase portions of the complex signal  
at a first-phase sampling time and at a second-phase sampling time separated from the first-phase  
sampling time by an offset;

35                separating the sampled first-phase signal into a sample-time data stream and a time-  
offset data stream;

              making a tentative symbolic decision on signals from the first-phase sample-time  
data stream;

              combining the tentative decisions with signals from the first-phase sample-time

- 1 data stream to generate a symbolic first-phase error term;  
multiplying the symbolic first-phase error term with a signal representing the time-  
offset sampled signal of the second-phase portion of the complex signal.
- 5 31. The method according to claim 30, further comprising:  
separating the sampled second-phase signal into a sample-time data stream and a  
time-offset data stream;  
making a tentative symbolic decision on signals from the second-phase sample-time  
data stream;  
10 combining the tentative decisions with signals from the second-phase sample-time  
data stream to generate a symbolic second-phase error term;  
multiplying the symbolic second-phase error term with a signal representing the  
time-offset sampled signal of the first-phase portion of the complex signal.
- 15 32. The method according to claim 30, further comprising:  
defining a phase error term, representing the result of the multiplication of the  
symbolic first-phase error term with the time-offset sampled signal representing the second-phase  
portion of the complex signal; and  
controlling a reference synthesizer to provide phase correction signals to a phase  
20 correction circuit in operative response to the phase error term.
33. The method according to claim 32, wherein the first-phase and second-phase  
portions of the complex signal are its in-phase and quadrature-phase components.
- 25 34. The method according to claim 33, wherein an in-phase sample-time signal  
corresponds to a quadrature-phase time-offset signal and a quadrature-phase sample-time signal  
corresponds to an in-phase time-offset signal.
- 30 35. The method according to claim 30, wherein the signal representing the time-offset  
sampled signal of second-phase portion of the complex signal is the sign of the time-offset  
sampled signal.
36. The method according to claim 30, wherein the step of separating the sampled first-  
phase signal into a sample-time data stream and a time-offset data stream comprises taking the  
35 Hilbert transform of the first-phase sample-time data stream.
37. An integrated circuit comprising:  
a decision directed symbol error magnitude determination circuit;

1                   a symbol rotation direction indication circuit; and  
                  wherein the symbol error magnitude circuit operative in response to a first-phase  
portion of a complex signal, the symbol rotation direction indication circuit operative in response  
to a second-phase portion of the complex signal, the first-phase and second-phase portions offset  
5                   from one another.

38.   An integrated circuit comprising:  
          a decision directed symbol error magnitude determination circuit;  
          a symbol rotation direction indication circuit; and  
10           wherein the symbol error magnitude circuit operative in response to a first-phase  
portion of a complex signal, the symbol rotation direction indication circuit operative in response  
to a Hilbert transform of the first-phase portion.

39.   The integrated circuit according to claim 37, the decision directed symbol error  
15       magnitude circuit further comprising:  
          a first-phase signal;  
          a decision circuit outputting first-phase decisions; and  
          an error circuit summing an first-phase decision with a first-phase signal to define  
a first-phase error term.

20                   40.   The integrated circuit according to claim 39, the symbol rotation direction  
indication circuit further comprising:  
          a signal representing a second-phase midpoint signal; and  
          a combining circuit, combining the first-phase error term with the signal  
25       representing the second-phase midpoint signal.

41.   The integrated circuit according to claim 40, wherein the first-phase signal is an in-  
phase component of an offset complex signal.

30                   42.   The integrated circuit according to claim 41, wherein the second-phase midpoint  
signal is a quadrature-phase component of an offset complex signal.

43.   The integrated circuit according to claim 42, wherein the signal representing the  
quadrature-phase midpoint signal is the sign of the quadrature-phase midpoint signal.

35                   44.   The integrated circuit according to claim 43, wherein the quadrature-phase midpoint  
signal corresponds to an offset quadrature-phase signal sampled at an in-phase sample time.

1

5

10

15

20

25

30

35

45. A method of operating an integrated circuit, comprising:  
providing a decision directed symbol error magnitude circuit;  
providing a symbol rotation direction indication circuit; and  
wherein the symbol error magnitude circuit operative in response to a first-phase  
portion of a complex signal, the symbol rotation direction indication circuit operative in response  
to a second -phase portion of the complex signal, the first-phase and second-phase portions offset  
from one another.

46. A method of operating an integrated circuit, comprising:  
providing a decision directed symbol error magnitude circuit;  
providing a symbol rotation direction indication circuit; and  
wherein the symbol error magnitude circuit operative in response to a first-phase  
portion of a complex signal, the symbol rotation direction indication circuit operative in response  
to a Hilbert transform of the first-phase portion.

47. The method according to claim 45, further comprising:  
providing a first-phase signal;  
providing first-phase decisions from a decision circuit; and  
summing a first-phase decision with a first-phase signal to define a first-phase error  
term.

48. The method according to claim 47, further comprising:  
providing a signal representing a second-phase midpoint signal; and  
combining the first-phase error term with the signal representing the second-phase  
midpoint signal to define a phase error term.

49. An integrated circuit receiver comprising:  
at least one timing loop;  
a decision feedback equalizer including;  
a feedforward filter; and  
a decision feedback filter; and  
a maximum likelihood sequence estimation circuit, coupled to receive input symbol  
samples from the feedforward filter, the maximum likelihood sequence estimation circuit  
integrated into the timing loop so as to provide enhanced reliability symbolic decisions to an  
input of the timing loop.

1           50. The integrated circuit receiver according to claim 49, the receiver operating on a complex signal transmitted in accordance with an 8-VSB modulation scheme, the receiver further comprising:

5               a summing circuit coupled in parallel fashion across the maximum likelihood sequence estimation circuit, the summing circuit combining input signal samples with symbolic decision output from the sequence estimation circuit to define a sequence estimated error term.

10           51. The integrated circuit receiver according to claim 50, wherein the feedforward filter includes adaptively updateable coefficient taps, the sequence estimated error term being provided to the feedforward filter to drive the tap updates.

15           52. The integrated circuit receiver according to claim 50, wherein the decision feedback filter includes adaptively updateable coefficient taps, the sequence estimated error term being provided to the decision feedback filter to drive the tap updates.

20           53. The integrated circuit receiver according to claim 50, wherein the maximum likelihood sequence estimation circuit is a trellis decoder, the trellis decoder including:

              a decision device, receiving input symbol samples from the feedforward filter;  
              a path metric circuit for tracking a symbol sample's time history and for  
25           determining a symbolic decision likelihood based on a symbol sample's historical sequence; and  
              a path traceback circuit for storing a plurality of sequential symbolic decisions, the output of the traceback circuit outputting at least a final decision corresponding to a maximum symbolic decision likelihood based on a symbol sample's historical sequence.

30           54. The integrated circuit receiver according to claim 53, the traceback circuit coupled to output each of a plurality of intermediate symbolic decisions, each corresponding to a particular symbolic decision along the sequence.

35           55. The integrated circuit receiver according to claim 54, the traceback circuit having a length N, wherein N corresponds to the number of symbolic decision estimations within a sequence, each estimation represented by a circuit delay  $1/N$ , each of the plurality of intermediate symbolic decisions separated from one another in time by an integer relationship with  $1/N$ .

              56. The integrated circuit receiver according to claim 55, wherein selected ones of the plurality of intermediate symbolic decisions are chosen for outputting based on a characteristic total delay of each selected one.



- 1           57.   The integrated circuit receiver according to claim 56, further comprising:  
            a carrier recovery loop operating to detect a difference in phase or frequency  
between a signal input to the trellis decoder and a symbolic decision output from the trellis  
decoder;  
5           wherein the decision feedback filter provides a compensation signal based on a  
symbolic decision output from the trellis decoder; and  
            wherein the carrier recovery circuit operates on an intermediate symbolic decision  
occurring earlier in the sequence than the symbolic decision provided the decision feedback filter.
- 10          58.   The integrated circuit receiver according to claim 56, further comprising a timing  
recovery loop operating to detect a difference in phase or frequency between a signal input to the  
trellis decoder and a symbolic decision output from the trellis decoder wherein the carrier  
recovery circuit operates on an intermediate symbolic decision occurring earlier in the sequence  
than symbolic decision provided the timing recovery loop.
- 15          59.   In an integrated circuit receiver, a method for operating a decision feedback  
equalizer, the method comprising:  
            providing a maximum likelihood sequence estimation circuit, including a symbolic  
traceback memory, the maximum likelihood sequence estimation circuit coupled to receive input  
20          symbol samples from a feedforward filter;  
            inputting a symbolic decision, representing a best survivor path of the symbolic  
traceback memory, to the decision feedback equalizer;  
            generating a sequence estimated symbolic error term from the best survivor path  
symbolic decision; and  
25          providing the sequence estimated symbolic error term to the decision feedback  
equalizer as a tap coefficient update signal.
60.   The method according to claim 59, wherein the maximum likelihood sequence  
estimation circuit includes:  
30          a decision device, receiving input symbol samples from the feedforward filter;  
            a path metric circuit for tracking a symbol sample's time history and for  
determining a symbolic decision likelihood based on a symbol sample's historical sequence; and  
            wherein the symbolic traceback memory stores a plurality of sequential symbolic  
decisions, the output of the traceback memory outputting at least a final decision corresponding  
35          to a maximum symbolic decision likelihood based on a symbol sample's historical sequence.
61.   The method according to claim 60, further comprising:  
            providing a symbolic decision, representing a best survivor path of the symbolic

- 1        traceback memory to an input of a timing recovery circuit;  
         detecting a difference in phase or frequency between the symbolic decision and an  
         input symbol sample; and  
         operating a de-rotator circuit in accordance with the comparison result.
- 5        62.    The method according to claim 61, wherein the symbolic traceback memory stores  
         a plurality of sequential symbolic decisions, the output of the traceback memory outputting at  
         least a final decision corresponding to a maximum symbolic decision likelihood based on a  
         symbol sample's historical sequence.
- 10       63.    The method according to claim 62, wherein the symbolic traceback memory is  
         further coupled to output a plurality of intermediate symbolic decisions, each corresponding to  
         a particular symbolic decision along the sequence.
- 15       64.    The method according to claim 63, the traceback circuit having a length N, wherein  
         N corresponds to the number of symbolic decision estimations within a sequence, each estimation  
         represented by a circuit delay  $1/N$ , each of the plurality of intermediate symbolic decisions  
         separated from one another in time by an integer relationship with  $1/N$ .
- 20       65.    The method according to claim 64, wherein selected ones of the plurality of  
         intermediate symbolic decisions are chosen for outputting based on a characteristic total delay  
         of each selected one.
- 25       66.    The method according to claim 65, wherein the timing recovery circuit operates on  
         an intermediate symbolic decision occurring earlier in the sequence than the symbolic decision  
         provided the decision feedback filter.
- 30       67.    An integrated circuit receiver, including an adaptive decision feedback equalizer,  
         comprising:  
         a feedforward filter;  
         a decision circuit;  
         a decision feedback filter coupled in parallel fashion with the decision circuit; and  
         an offset generation circuit, wherein the offset generation circuit provides an offset  
         signal to an output signal from the decision feedback filter, the offset signal corresponding to a  
35       bitwise representation of a DC component.
68.    The integrated circuit receiver according to claim 67, further comprising:  
         a complex input signal corresponding to a multi-level constellation of symbols,

- 1 each symbol represented by a number of bits; and  
wherein the number of bits representing each symbol is determined by a power of  
two which identifies a size of the constellation.
- 5 69. The integrated circuit receiver according to claim 68, wherein the bit representation  
of the constellation includes a fixed offset term.
70. The integrated circuit receiver according to claim 69, wherein the fixed offset term  
is capable of representation by adding an additional bit to each number bits representing a  
10 symbol.
71. The integrated circuit receiver according to claim 70, wherein the offset signal  
corresponds to a digital value determined by the additional bit.
- 15 72. The integrated circuit receiver according to claim 71, wherein the constellation is  
a 256-QAM constellation and the number of bits representing each symbol is four, the offset  
signal corresponding to a  $-1/2$  bit offset in the representation of QAM signals.
73. An integrated circuit receiver operating on a constellation of complex symbols,  
20 each symbol represented by a number  $N$  of bits, the receiver comprising:  
an adaptive decision feedback equalizer including:  
a decision feedback filter, constructed to receive a symbol decision having a  
wordlength of  $N-1$  bits, the decision feedback filter outputting a compensated symbol decision  
having a wordlength of  $N-1$  bits;  
25 an offset generation circuit, generating a DC value corresponding to an  $N$ th bit  
representation; and  
a summing circuit for combining the decision feedback filter output and the DC  
value generated by the offset generation circuit.
- 30 74. The integrated circuit receiver according to claim 73, wherein the offset generation  
circuit is a filter.
75. The integrated circuit receiver according to claim 74, further comprising:  
a feedforward filter; and  
35 a decision circuit, coupled in parallel fashion with the decision feedback filter, the  
decision circuit outputting an  $N-1$  bit wide word representing symbol decisions and a symbol  
error term.

- 1           76. The integrated circuit receiver according to claim 75, wherein the symbol error term adaptively trains filter coefficients of the decision feedback filter, the decision feedback filter coefficients provided to the offset generation circuit.
- 5           77. An integrated circuit receiver operating on a constellation of complex symbols, each symbol capable of representation by a digital word having a wordlength N of bits, the receiver comprising:
- a feedback filter, constructed to receive an input stimulus signal having a wordlength of N-1 bits the feedback filter outputting a signal having a wordlength of N-1 bits;
- 10           a correction filter constructed to provide an output signal having a single bit representation; and
- means for combining the feedback filter output and the correction filter output to define a signal having a value consistent with an N-bit representation.
- 15           78. The integrated circuit receiver according to claim 77, wherein the correction filter outputs a signal corresponding to a fixed offset term introduced by a representation of complex symbols in a first numbering system.
79. The integrated circuit receiver according to claim 77, wherein the correction filter
- 20           outputs a signal corresponding to a fixed offset term introduced by a pilot tone inserted into a transmitted spectrum.
80. The integrated circuit receiver according to claim 77, wherein the correction filter
- 25           outputs a signal corresponding to a fixed offset term representing the sum of a fixed offset introduced by a representation of complex symbols in a first numbering system and a fixed offset introduced by a pilot tone inserted into a transmitted spectrum.
81. The integrated circuit receiver according to claim 77, further comprising:
- a feedforward filter; and
- 30           a decision device, coupled in parallel fashion with the feedback filter, the decision device outputting symbolic decisions in an N-1 bit representation and further outputting a symbolic error term associated with each decision.
82. The integrated circuit receiver according to claim 81, wherein the symbolic error
- 35           term adaptively trains filter coefficients of the feedback filter, the feedback filter providing an ISI compensation to symbolic decisions expressed in an N-1 bit representation.
83. The integrated circuit receiver according to claim 82, wherein the correction filter

1 receives filter coefficients from the feedback filter, the correction filter providing an ISI compensation to a fixed offset term.

5 84. The integrated circuit receiver according to claim 83, the constellation comprising a 256-QAM constellation, each real and each imaginary symbol represented by a 5-bit word in two's complement notation, the 5-bit word comprising a 4-bit portion expressing each symbol's relative position within the constellation and a 1-bit portion expressing a fixed offset between each symbol's relative position and its absolute position within the constellation.

10 85. In an integrated circuit receiver, a method for adaptively equalizing symbols expressed as a digital word, the method comprising:

identifying a nibble component of the word, the nibble component representing a fixed offset value;  
truncating the word to a vestigial representation excluding the nibble component;  
15 convolving the vestigial representation with coefficient taps in a first filter;  
convolving the fixed offset value, corresponding to the excluded nibble component, with coefficient taps in a second filter; and  
summing the convolutions.

20 86. The method according to claim 85, wherein the first filter is a decision feedback filter.

87. The method according to claim 86, wherein the second filter is a DC correction filter.

25 88. A digital communication system for receiving signals modulated in accordance with a multiplicity of modulation formats, comprising:

a front end receiving an input spectrum at an intermediate frequency;  
first and second nested carrier tracking loops, the first loop acquiring carrier frequency lock in operative response to a predetermined frequency component inserted into the received spectrum, the second loop providing a signal adapted to position the spectrum at a predetermined location relative to baseband in operative response to said predetermined frequency component;

30 a third tracking loop coupled to define a symbol timing parameter in operative response to said same predetermined frequency component;

35 an equivalent filter operating on the received spectrum in order to define a pair of symmetric signals, each of the symmetric signals centered at the characteristic frequency of the predetermined frequency component when the received spectrum is at baseband;

1                   a decision directed carrier phase recovery loop having a phase detector operative  
with respect to each of the multiplicity of modulation formats;  
                  a single bit LMS derotator coupled to adjust phase offset of signals directed to an  
adaptive decision feedback equalizer;  
5                   an adaptive decision feedback equalizer, including;  
                  a feedforward filter;  
                  a decision feedback filter; and  
                  a maximum likelihood sequence estimation circuit, coupled to receive input symbol  
samples from the feedforward filter, the maximum likelihood sequence estimation circuit  
10                  integrated into a timing loop so as to provide enhanced reliability symbolic decisions to an input  
of the timing loop.

89.   The digital communication system according to claim 88, wherein the multiplicity  
of modulation formats includes vestigial sideband modulation (VSB), quadrature amplitude  
15       modulation (QAM) and offset-quadrature amplitude modulation (OQAM).

90.   The digital communication system according to claim 89, further comprising:  
          a first derotator, coupled into the signal path in a position after the front end, the  
derotator converting the received spectrum to a position relative to baseband signal in response  
20       to the first tracking loop;  
          a variable rate interpolator;  
          an NTSC interference rejection filter;  
          a square root Nyquist filter, coupled into the signal path in a position after the  
NTSC interference rejection filter; and  
25       a second derotator coupled into the signal path in a position after the square root  
Nyquist filter, the second derotator adjusting the received spectrum to a baseband signal in  
response to the second tracking loop.

91.   The digital communication system according to claim 90, further comprising a  
30       Nyquist prefilter, coupled in parallel to the signal path and in a position after the second  
derotator, the Nyquist prefilter and the square root Nyquist filter defining the equivalent filter.

92.   The digital communication system according to claim 91, further comprising:  
          a real to imaginary signal converter, the converter operative to create an imaginary  
35       analogue to a real signal, the imaginary analogue having a same time stamp as the real signal; and  
          a time compensation circuit, coupled to time shift an imaginary component of a  
signal in one modulation format into an imaginary component of a signal in another modulation  
format.

1           93. The digital communication system according to claim 92, wherein the real to  
imaginary signal converter is a Hilbert transform filter coupled to define a Q analogue signal  
from an I rail signal.

5           94. The digital communication system according to claim 93, wherein the time  
compensation circuit is a Z transform circuit, having a characteristic delay  $Z^{-1/2}$ .

          95. The digital communication system according to claim 94, wherein the characteristic  
delay  $Z^{-1/2}$  is equal to one half a symbol time of a QAM signal.

10          96. A digital communication system for receiving signals modulated an accordance  
with a multiplicity of modulation formats, comprising:

          a front end receiving an input spectrum at an intermediate frequency;

          first and second nested carrier tracking loops, the first loop acquiring carrier  
15 frequency lock in operative response to a pilot frequency component inserted into the received  
spectrum, the second loop providing a signal adapted to position the spectrum at a predetermined  
location relative to baseband in operative response to said pilot frequency component;

          a third tracking loop coupled to define a symbol timing parameter in operative  
response to said same pilot frequency component;

20          an equivalent filter operating on the received spectrum in order to define a pair of  
symmetric signals, each of the symmetric signals centered at the characteristic frequency of the  
pilot frequency component when the received spectrum is at baseband; and

          a decision directed carrier recovery loop having a phase detector operative with  
respect to each of the multiplicity of modulation formats.

25          97. The digital communication system according to claim 96, wherein the multiplicity  
of modulation formats includes vestigial sideband modulation (VSB), quadrature amplitude  
modulation (QAM) and offset-quadrature amplitude modulation (OQAM).

30          98. The digital communication system according to claim 97, the second tracking loop  
operative in conjunction with the first tracking loop to position the spectrum at a predetermined  
location relative to baseband when the spectrum represents a signal modulated in accordance with  
a first modulation format.

35          99. The digital communication system according to claim 98, the decision directed  
carrier loop operative in conjunction with the first tracking loop to position the spectrum at a  
predetermined location relative to baseband when the spectrum represents a signal modulated in  
accordance with a second modulation format.

1           100. The digital communication system according to claim 99, the decision directed  
carrier loop operative on input signals received from a maximum likelihood sequence estimation  
circuit integrated into an adaptive decision feedback equalizer.

5           101. A digital communication system for receiving signals modulated an accordance  
with a multiplicity of modulation formats, comprising:

a front end receiving an input spectrum at an intermediate frequency;

first and second nested carrier tracking loops;

a symbol timing loop; and

10           wherein the tracking and timing loops control reference synthesizer circuits in  
operative response to a passband signal centered at a frequency characteristic of an inserted pilot  
signal.

15           102. The digital communication system according to claim 101, wherein the passband  
signal comprises a pair of symmetric signals, each of the symmetric signals centered at the  
characteristic frequency of the pilot signal.

20           103. The digital communication system according to claim 102, wherein each of the  
symmetric signals includes an augmented pilot signal.

25           104. The digital communication system according to claim 103, wherein the passband  
signal is developed by an equivalent filter including a lowpass root Nyquist filter and a highpass  
Nyquist prefilter.

30

35

40



1/16

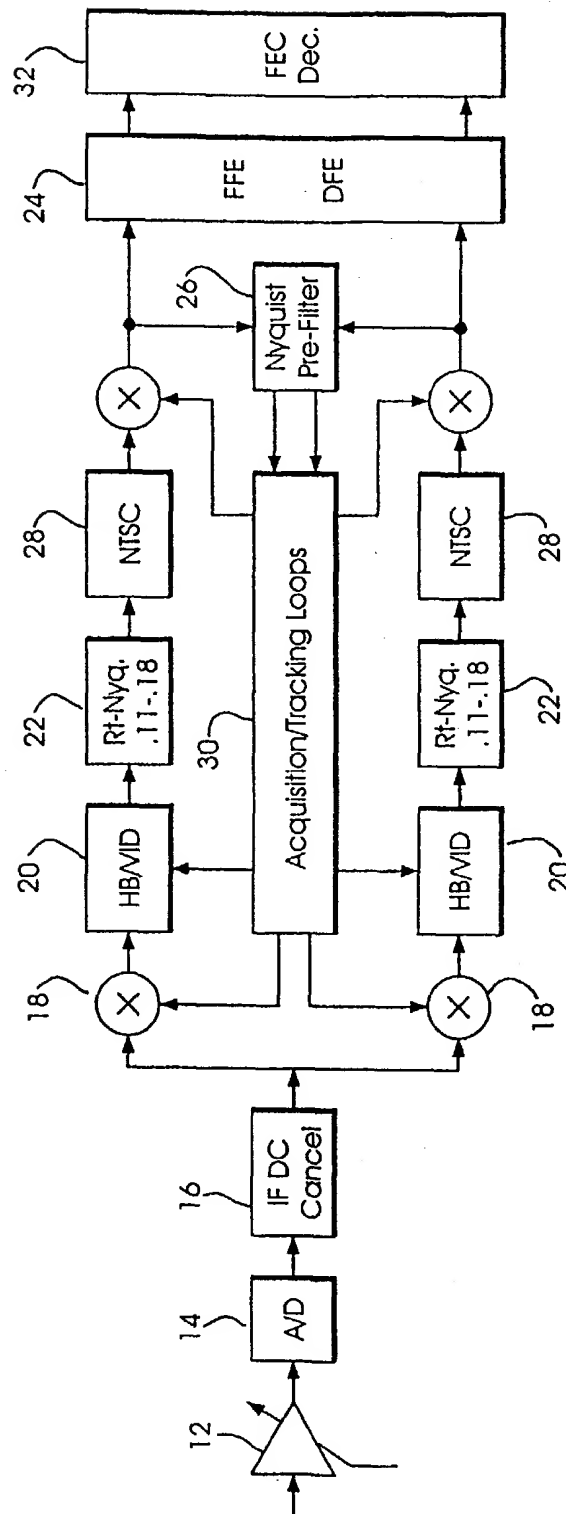


FIG. 1

2/16

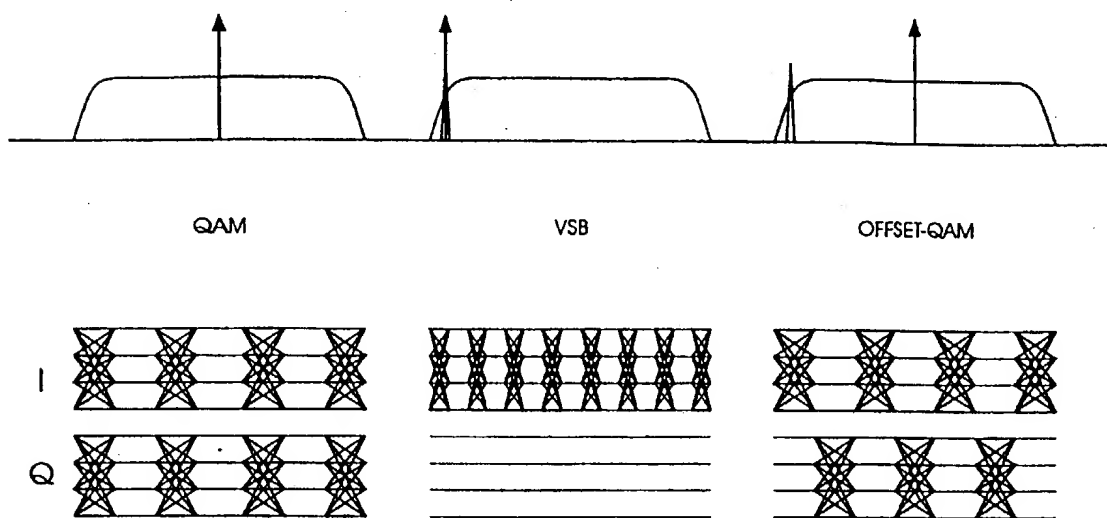


FIG. 2

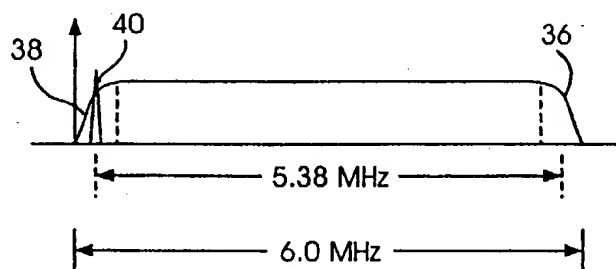


FIG. 3

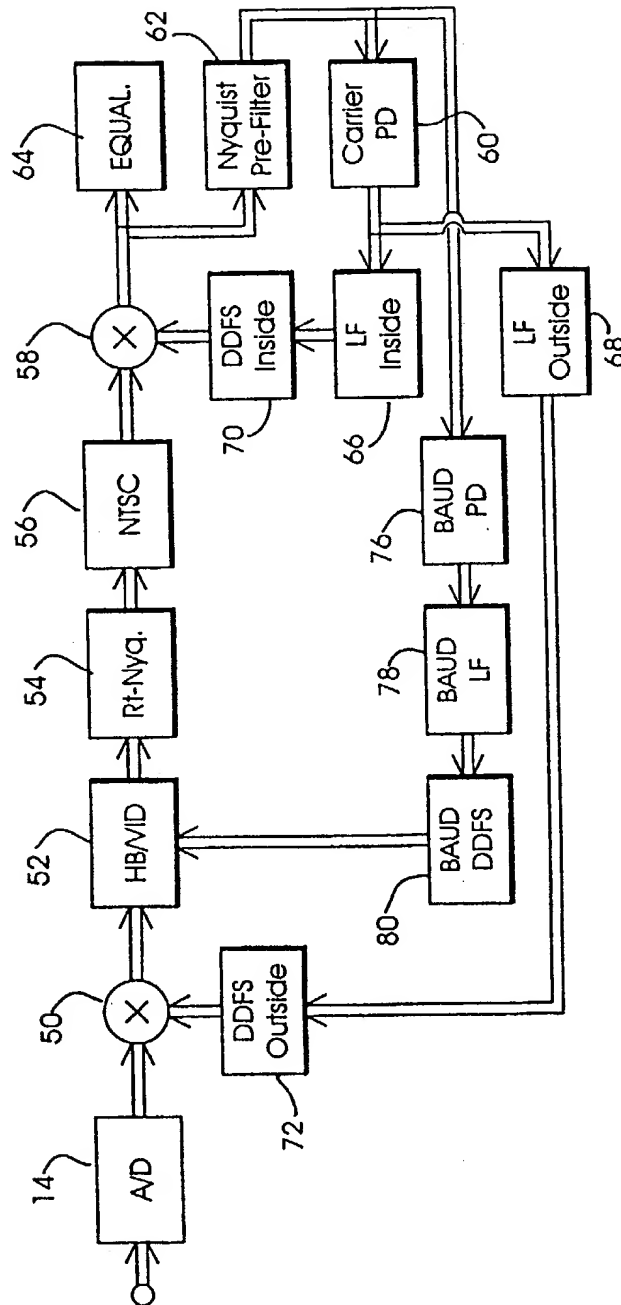


FIG. 4

4/16

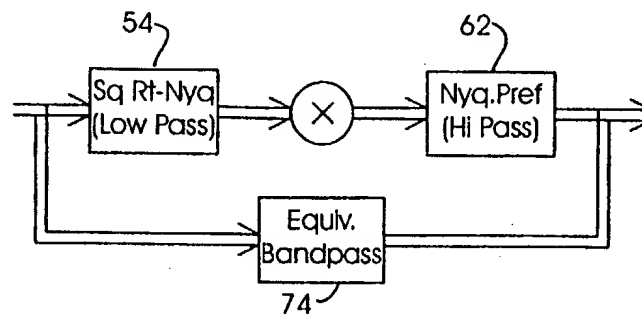


FIG. 5

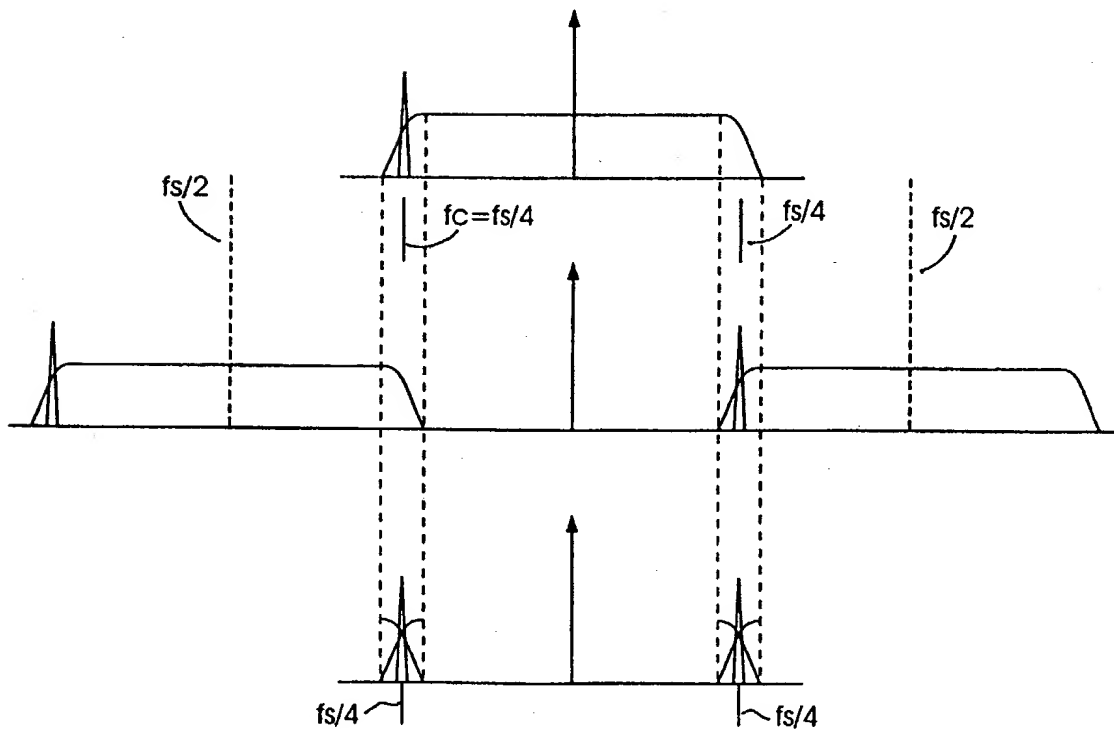


FIG. 6

5/16

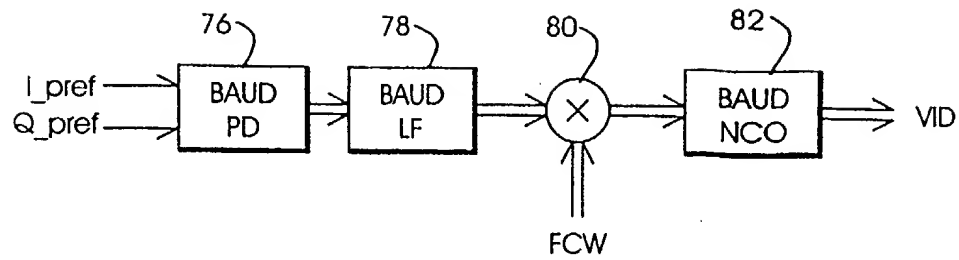


FIG. 7

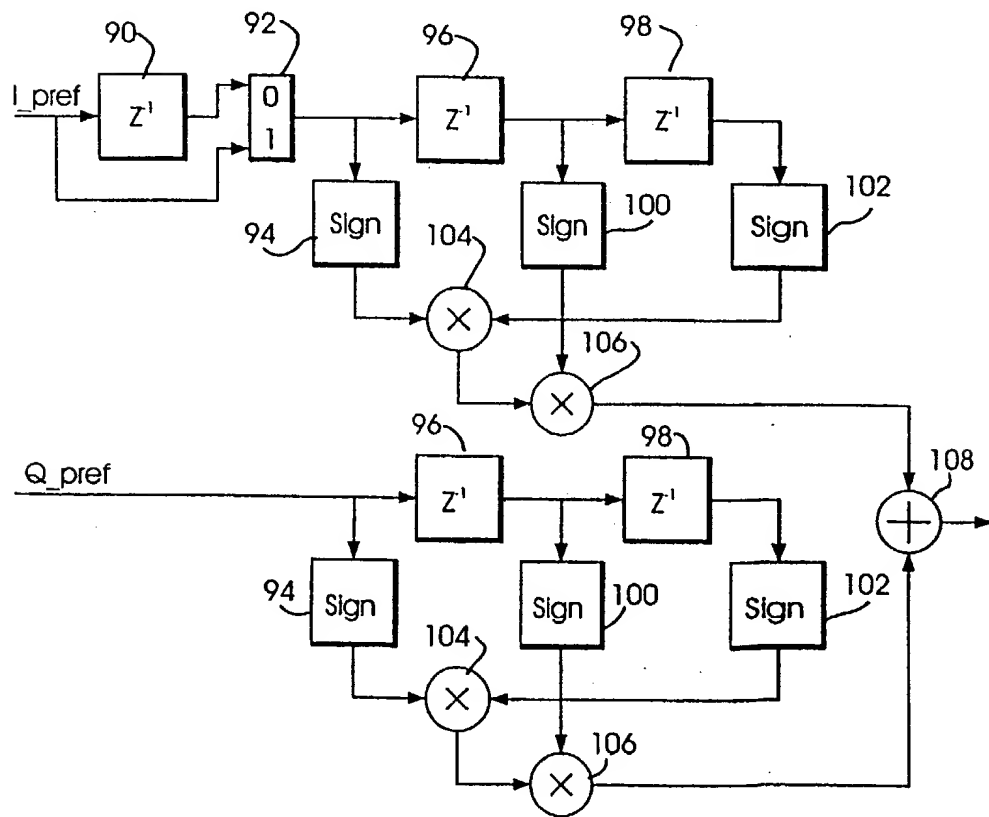


FIG. 8

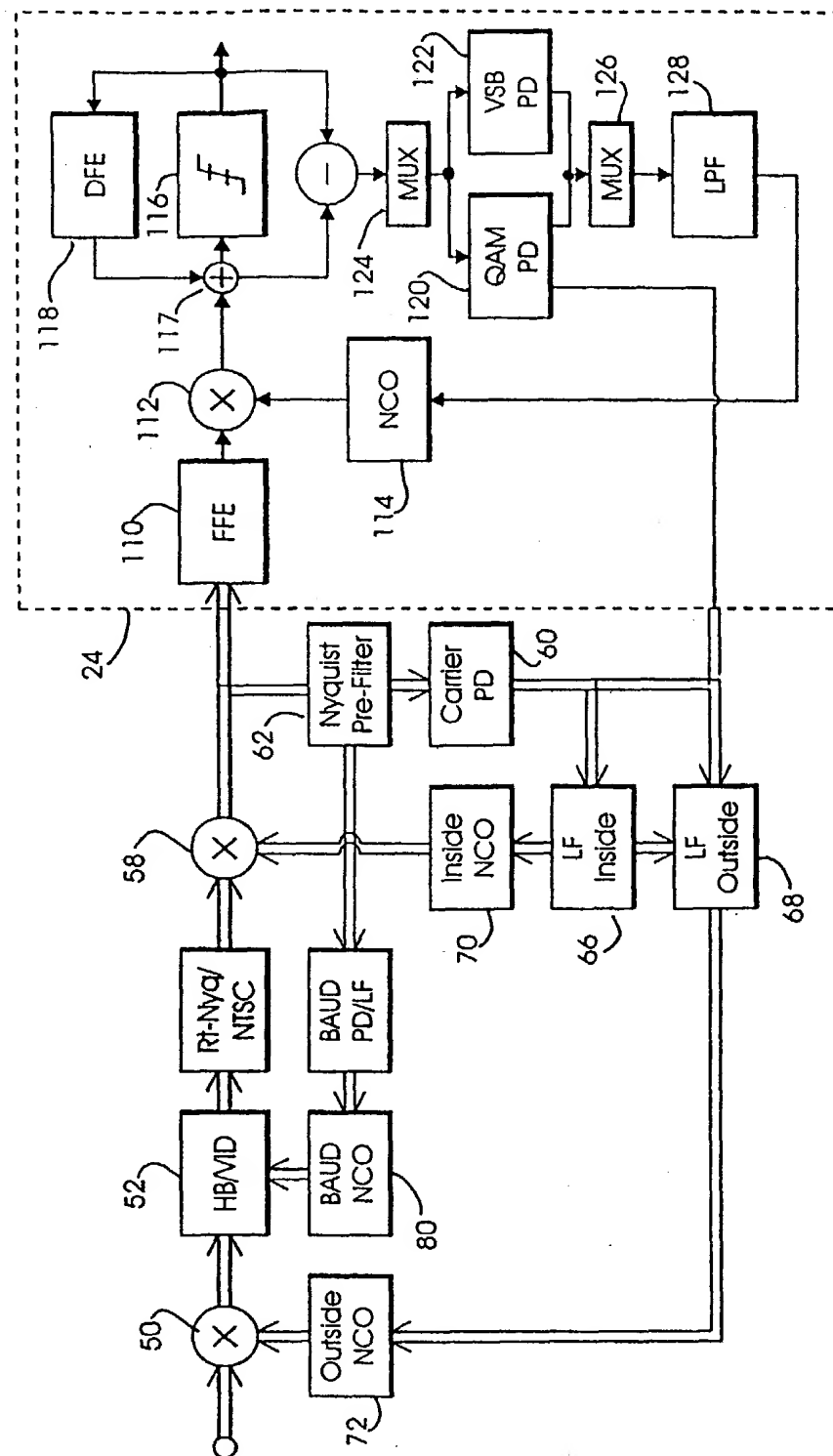


FIG. 9

7/16

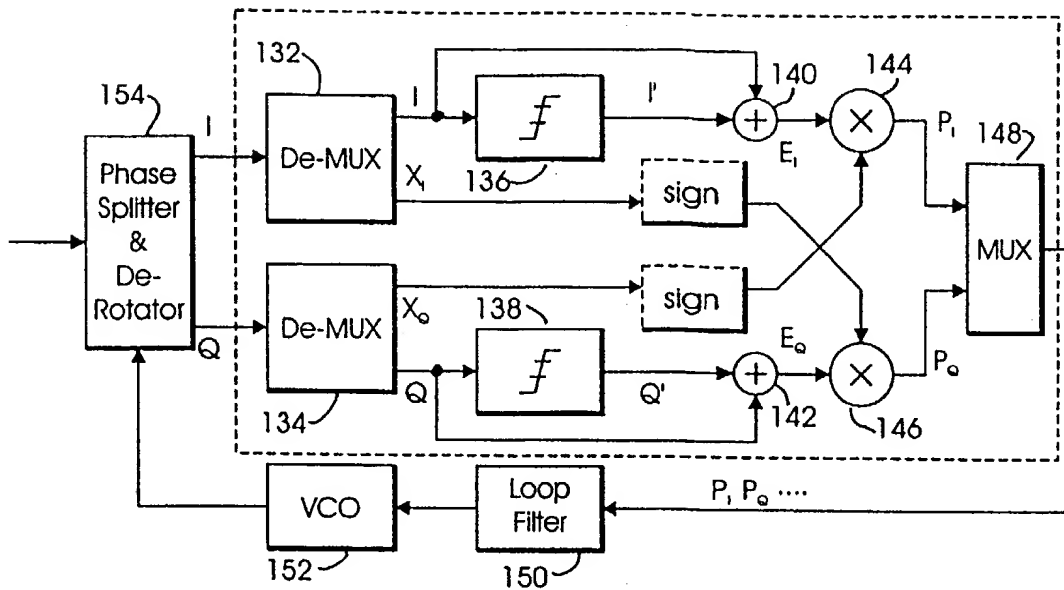


FIG. 10

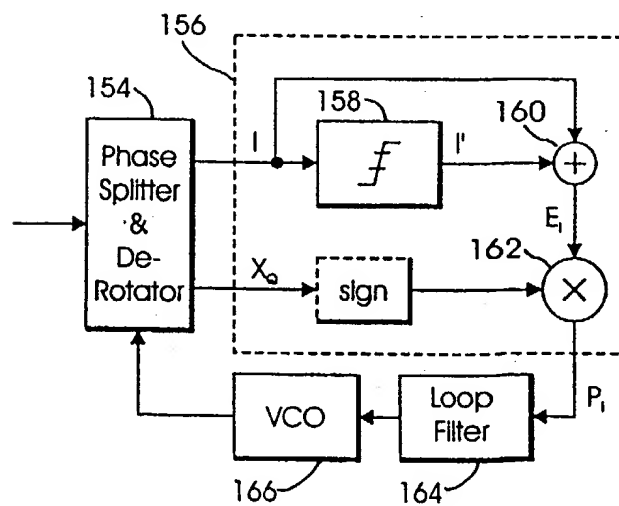


FIG. 11

8/16

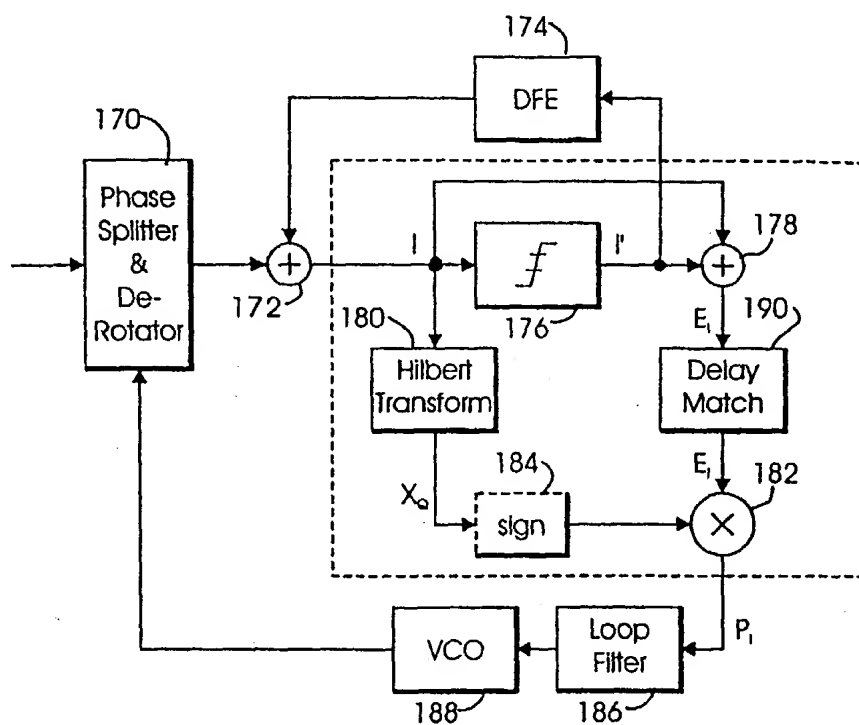


FIG. 12

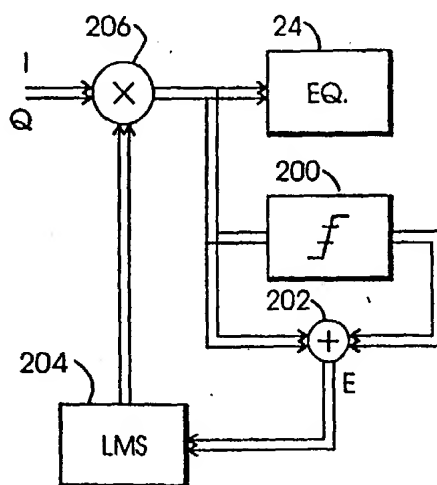


FIG. 13



9/16

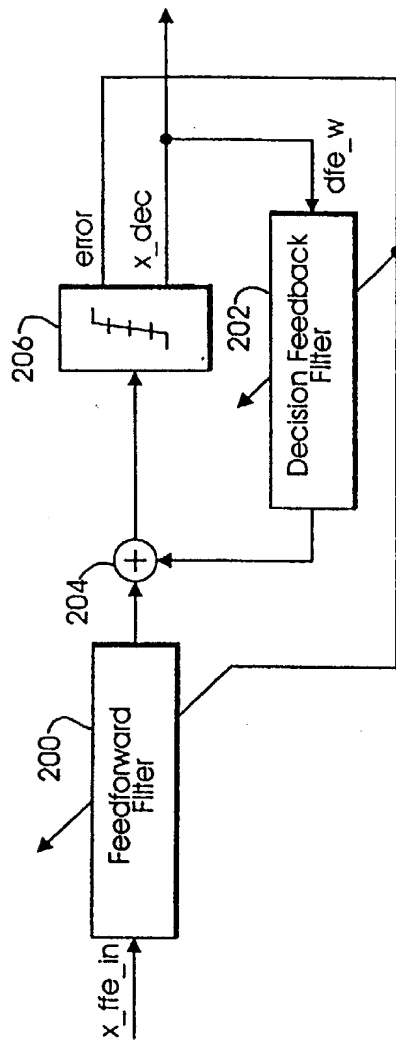
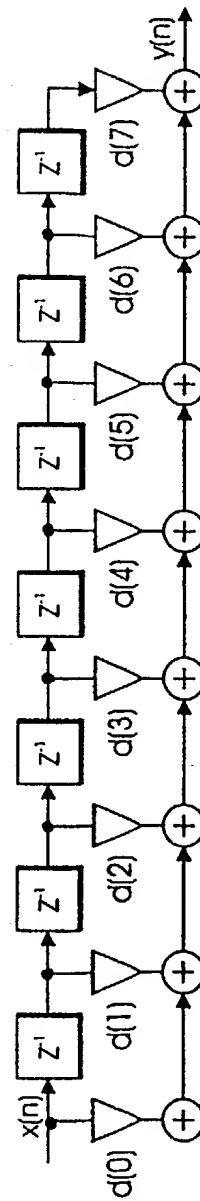


FIG. 14



$$y(n) = \sum_k d(k)x(n-k)$$

FIG. 15

10/16

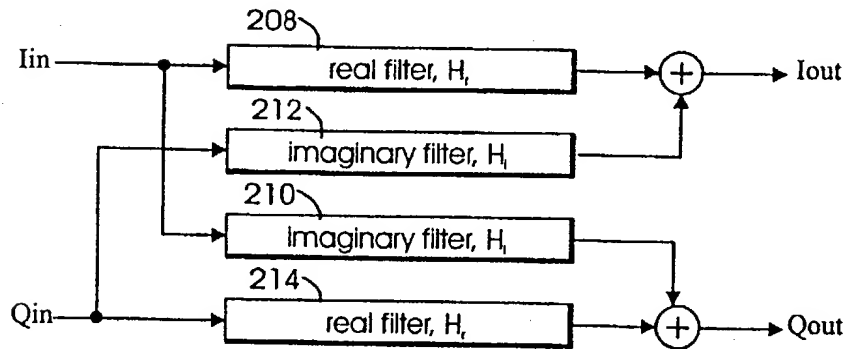


FIG. 16

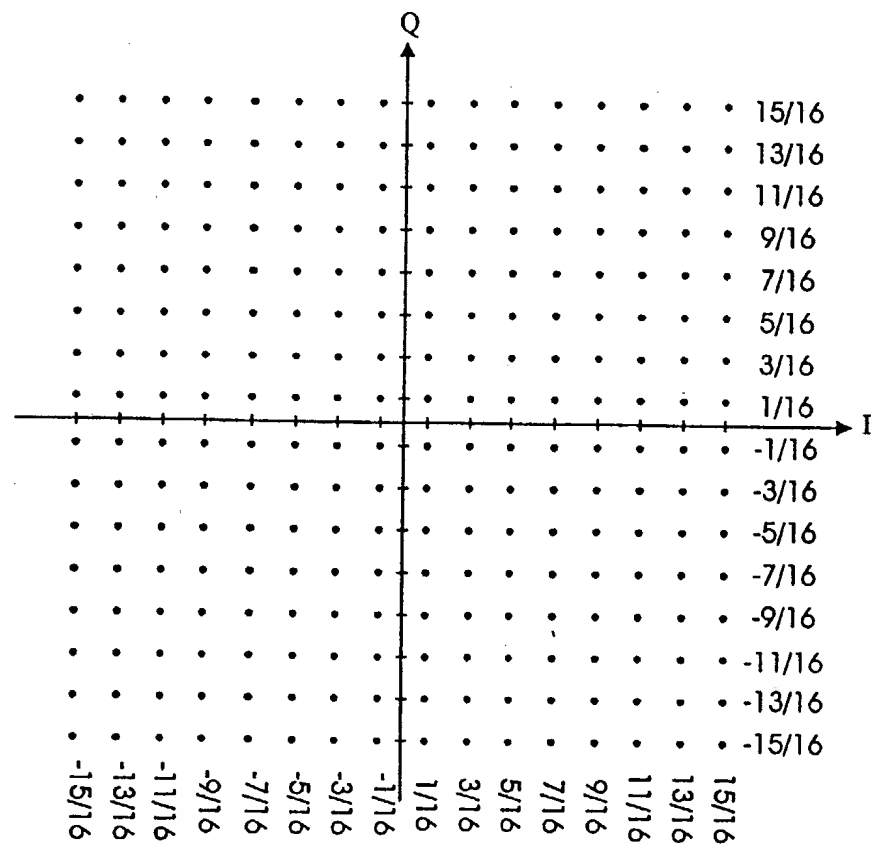


FIG. 17

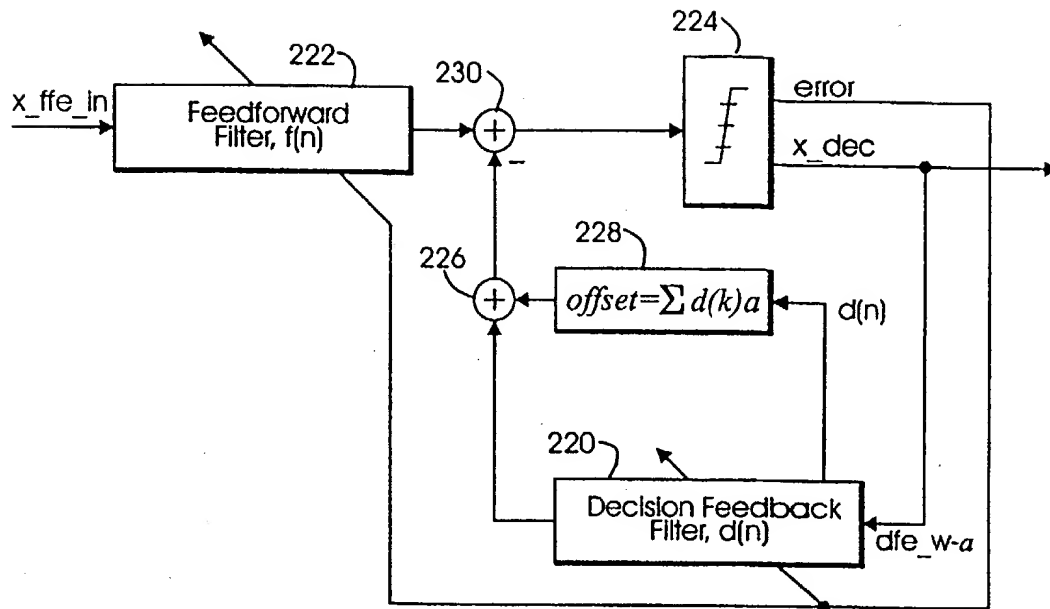


FIG. 18

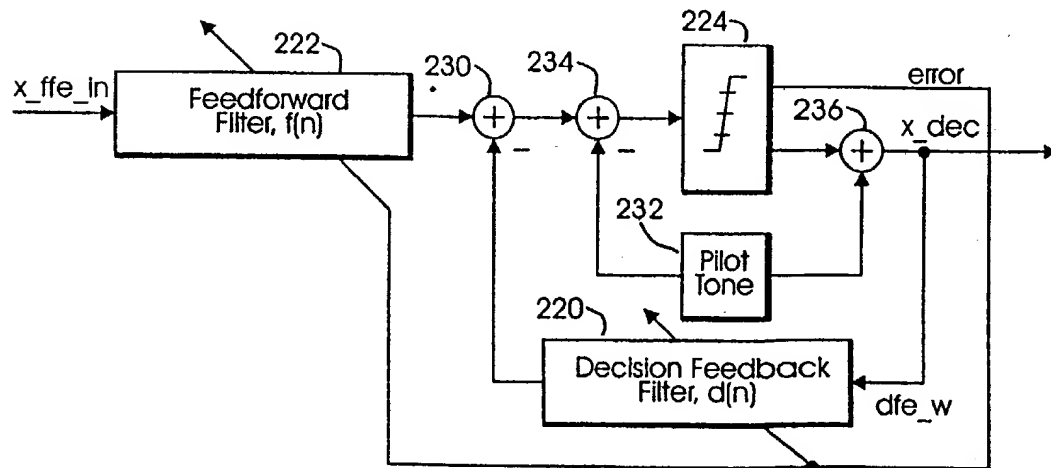


FIG. 19

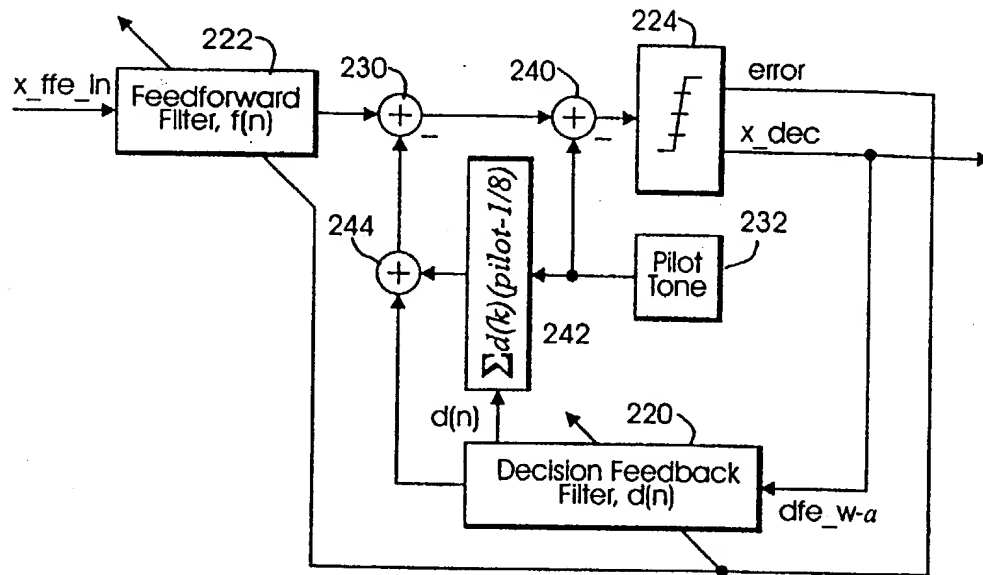


FIG. 20

13/16

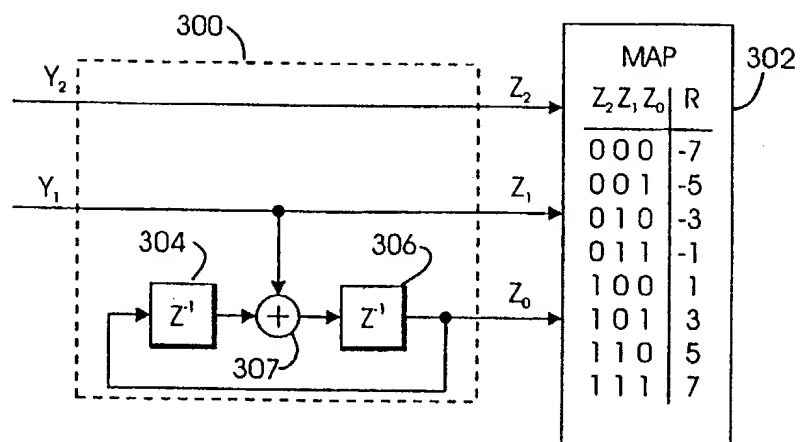


FIG. 21

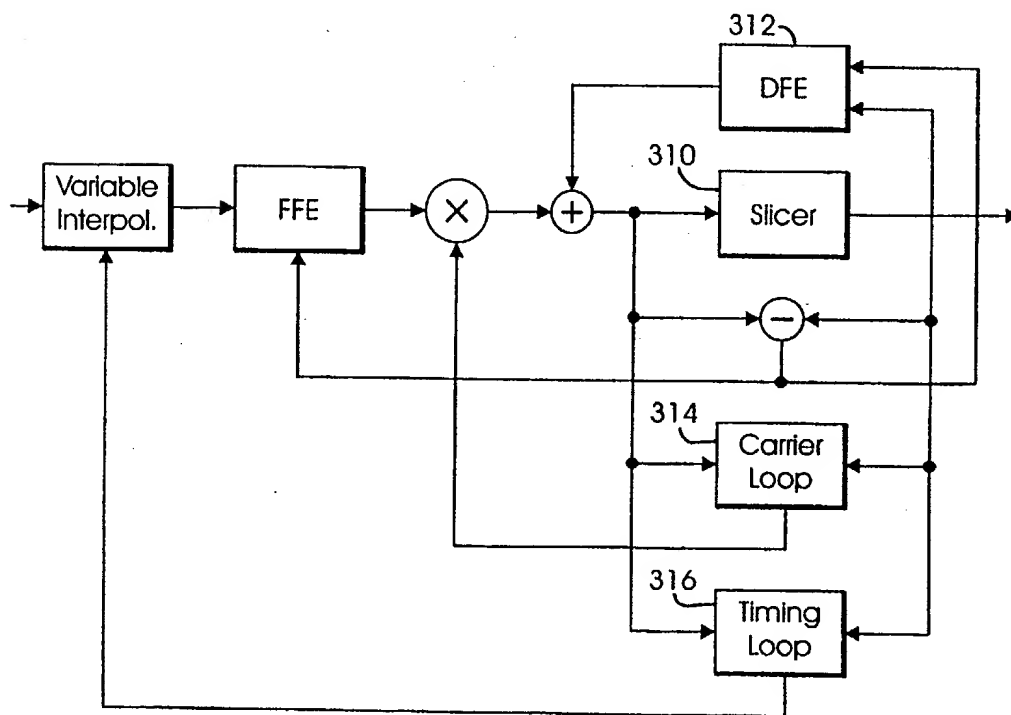


FIG. 22

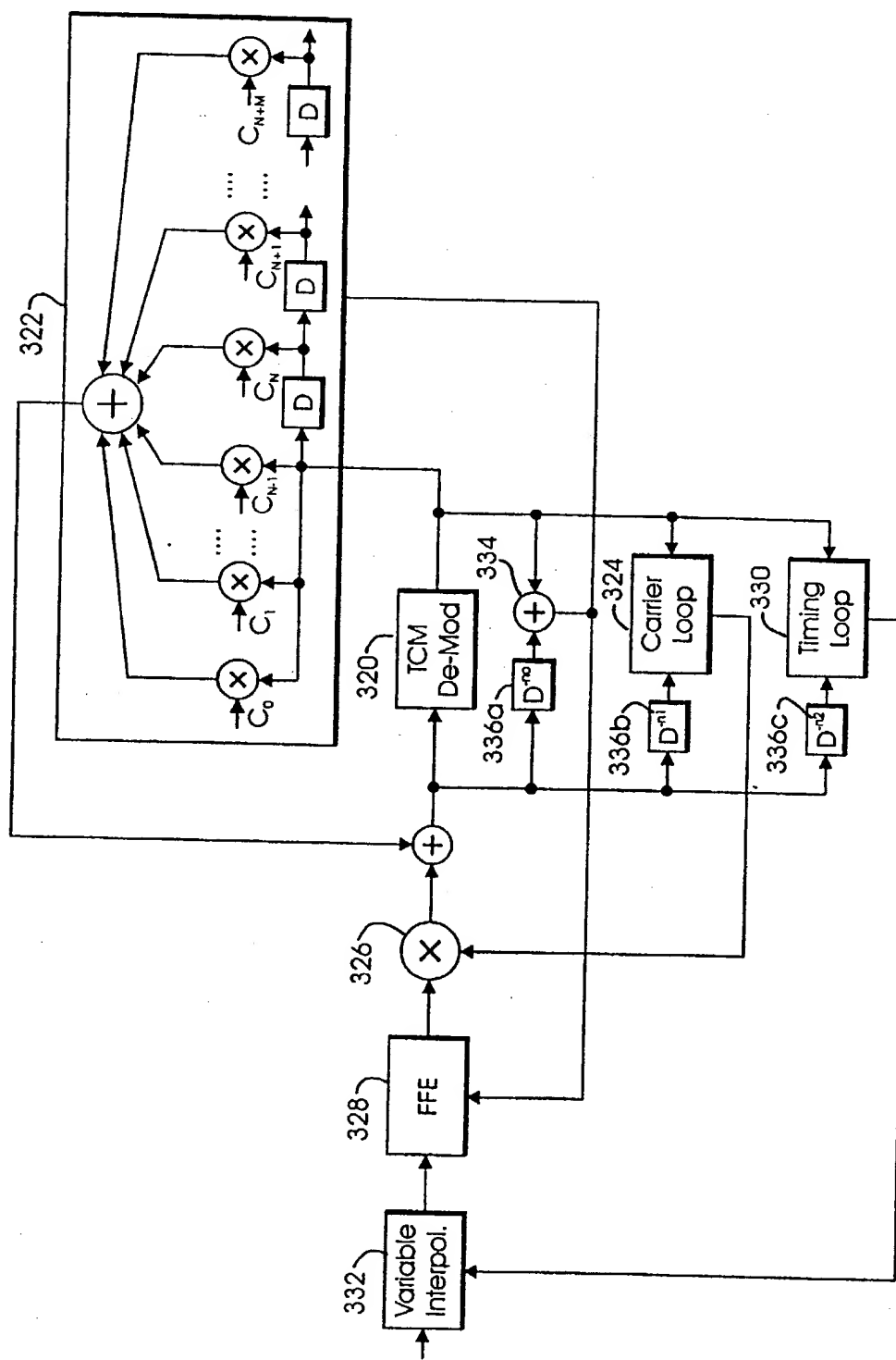


FIG. 23

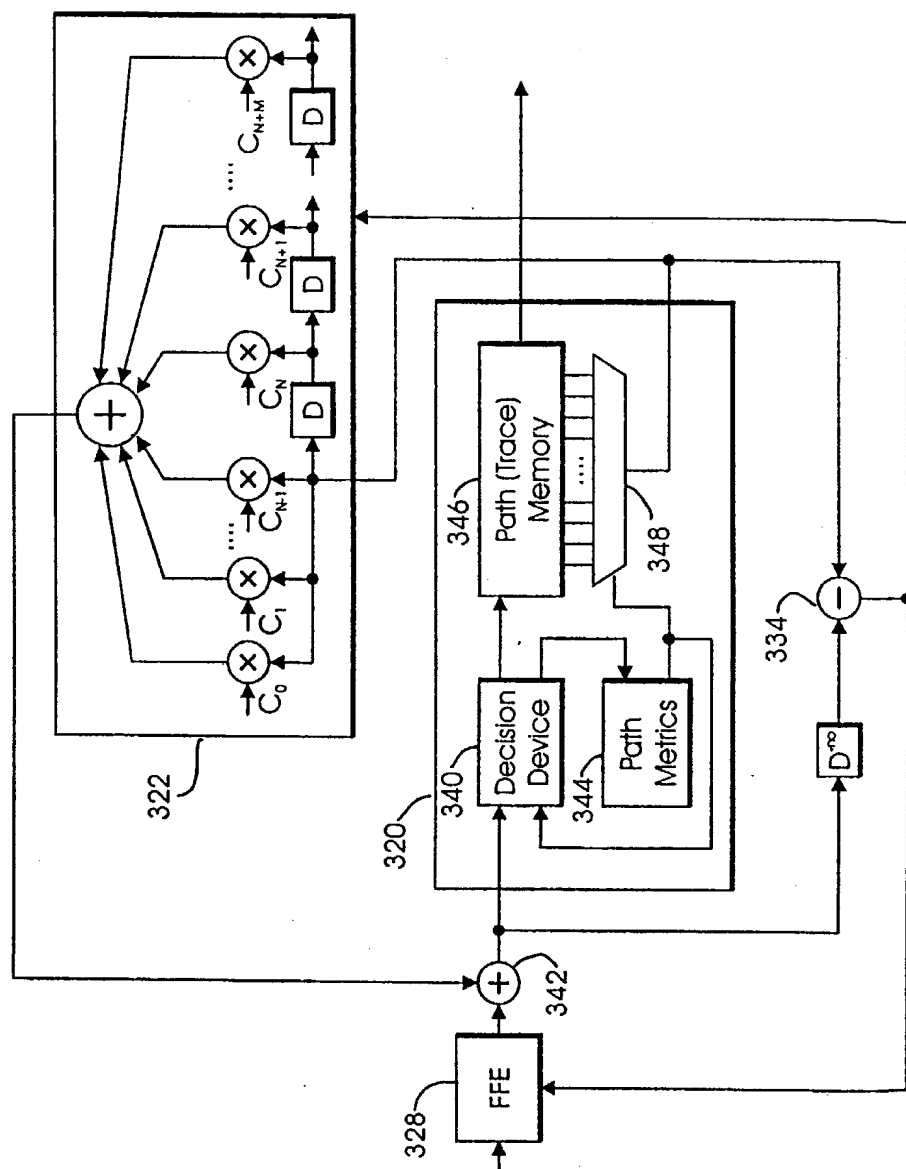


FIG. 24

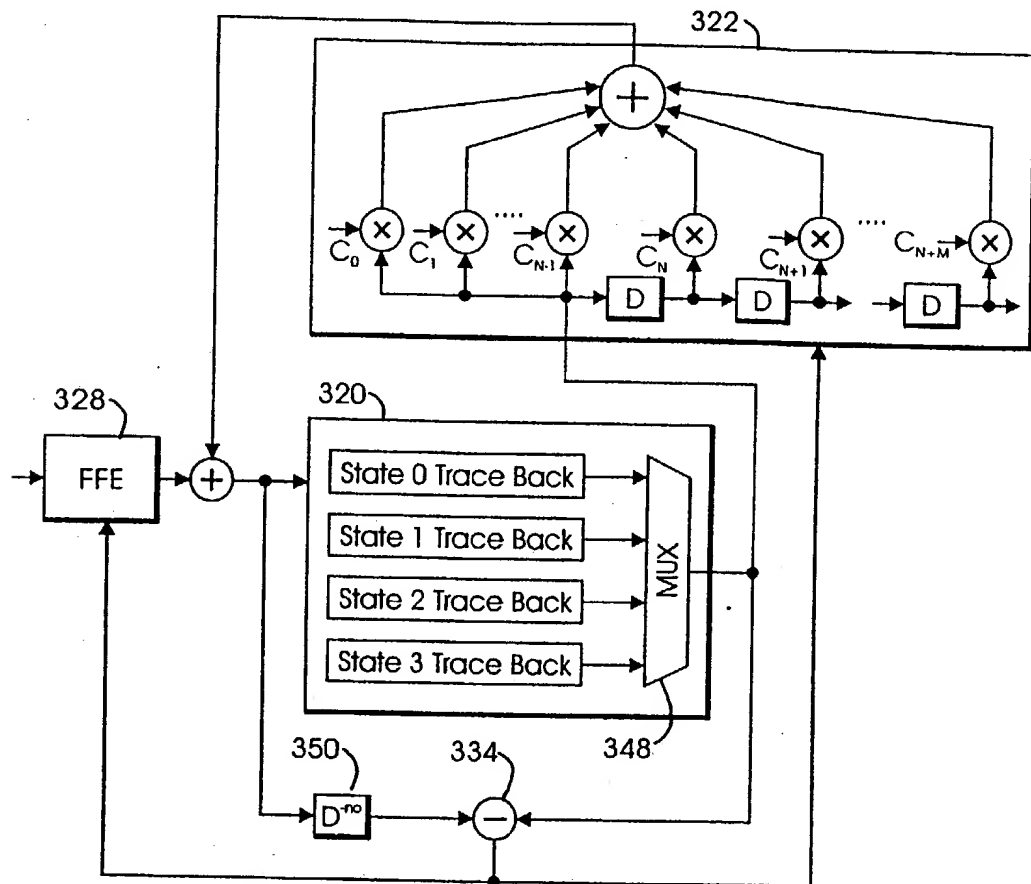


FIG. 25